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# Mantle plumes in the vicinity of subduction zones

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## Abstract

We present three-dimensional deep-mantle laboratory models of a compositional plume within the vicinity of a buoyancy-driven subducting plate with a fixed trailing edge. We modelled front plumes (in the mantle wedge), rear plumes (beneath the subducting plate) and side plumes with slab/plume systems of buoyancy flux ratio spanning a range from 2 to 100 that overlaps the ratios in nature of 0.2-100. This study shows that 1) rising side and front plumes can be dragged over thousands of kilometres into the mantle wedge, 2) flattening of rear plumes in the trench-normal direction can be initiated 700 km away from the trench, and a plume material layer of lesser density and viscosity can ultimately almost entirely underlay a retreating slab after slab/plume impact, 3) while side and rear plumes are not tilted until they reach  $\sim 600$  km depth, front plumes can be tilted at increasing depths as their plume buoyancy is lessened, and rise at a slower rate when subjected

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to a slab-induced downwelling, 4) rear plumes whose buoyancy flux is close to that of a slab, can retard subduction until the slab is 600 km long, and 5) slab-plume interaction can lead to a diversity of spatial plume material distributions into the mantle wedge. We discuss natural slab/plume systems of the Cascadia/Bowie-Cobb, and Nazca/San Felix-Juan Fernandez systems on the basis of our experiments and each geodynamic context and assess the influence of slab downwelling at depths for the starting plumes of Java, Coral Sea and East Solomon. Overall, this study shows how slab/plume interactions can result in a variety of geological, geophysical and geochemical signatures.

*Key words:*

subduction, mantle plume, analog modelling, mantle flow, slab rollback.

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## 1. Introduction

In the theory of plate tectonics, subduction zones and mantle plumes (hotspots) are described as two distinctive elements of mantle convection. Subduction carries cool oceanic lithosphere downward and plumes carry hot mantle from the deep interior toward the surface (Schubert, 2001). Hotspots have preferentially been located near divergent plate boundaries, and excluded from regions near convergent plate boundaries (e.g. Weinstein and Olson, 1989). However today's observations based mostly on tomographic studies suggest the presence of plumes in the vicinity of subduction zones (e.g. Obrebski et al., 2010). Such spatial proximity could have important geodynamic implications such as flattening of subduction (Dalziel et al., 2000), plume deflection, widespread magmatism (Geist & Richards, 1993), rapid

switches in tectonic modes, modified crustal growth (Wyman et al., 2002) and the formation of mineral deposits such as gold (Wyman et al., 1999).

Proposed examples of modern slab/plume interaction include the Cascadia subduction zone and the Yellowstone hotspot (Murphy et al., 1998; Smith et al., 2009), the Tonga subduction zone and the Samoa hotspot (Smith et al., 2001), and the Kamchatka subduction zone segment and the Kamchatka plume (Gorbatov et al., 2001). In the last 60 Myr, 29% and 17% of the commonly recognised mantle plumes have been within 1000 km and 500 km, respectively, of a subduction zone (Fletcher and Wyman, 2015). In the more distant geologic past, proposed examples include the interaction of the South Greenland and central Scandinavia subduction zones with a plume located between Baltica and Greenland at  $\sim 1284$ -1234 Ma (Söderlund et al., 2006), interaction of the retreating Gondwanan margin and the plume responsible for the Jurassic Karroo-Ferrar flood basalts (Dalziel et al., 2000), and the Mesoproterozoic plume-modified orogenesis in eastern Precambrian Australia (Betts et al., 2009).

Until recently, the different models that have been envisaged to explain the geological and geophysical observations have mostly been conceptual. For example, we know that mantle plumes can be deflected by mantle flow (Kerr and Mériaux, 2004) but the conditions under which a subducting plate captures a plume remain unknown. The influence of a mantle plume on a slab is not well known either. Such questions critically demand to be tested by dynamic models as they have clear importance in a number of geological environments.

Recently, Morishige et al. (2010) implemented two-dimensional numerical



38 simulations of a hot anomaly adjacent to a cold kinematically-driven down-  
 39 going slab to test the origin of a low velocity anomaly under the subducting  
 40 Pacific plate. Similarly, Lee and Lim (2014) used a two-dimensional model  
 41 of a cold kinematically-driven downgoing slab with a short-term temperature  
 42 anomaly into the mantle wedge to assess slab melting, and the occurrence  
 43 of the Abukuma adakite in northeastern Japan. Using three-dimensional  
 44 numerical simulations, Betts et al. (2012, 2015) modelled the behaviour of  
 45 subducting plates encountering a plume head prescribed, either at the base of  
 46 the subducting plate or at the base of the overriding plate, by a volume of  
 47 lesser density and viscosity. These studies quantified the manner in which a  
 48 plume head could modify trench and slab geometry. Besides those numerical  
 49 investigations, a small number of laboratory models have been presented.  
 50 Kincaid et al. (2013) and Druken et al. (2014) carried out experiments  
 51 with a rigid and kinematically driven subducting plate in interaction with a  
 52 thermal plume to model the bifurcation of the Yellowstone plume and the  
 53 entrainment of the Samoan plume in the Lau basin, respectively. Mériaux  
 54 et al. (2015a, 2015b) presented three-dimensional upper-mantle laboratory  
 55 models of the Gibraltar subduction zone and Canary plume, and the Manila  
 56 subduction zone and Hainan plume. These recent quantitative studies have  
 57 been significant steps forward in the understanding of slab/plume interac-  
 58 tion, but they were all case studies. Here we present the first generic study  
 59 of such interaction, as the stage for more systematic studies to come given  
 60 the complexity of the interaction.

61 In this paper, we report deep mantle laboratory analog experiments of  
 62 a compositional plume within the vicinity of a buoyancy-driven slab with a

fixed trailing plate. We present a set of 21 experiments, in which we vary the slab/plume buoyancy flux ratio over a range of 2-100 overlapping that of nature, and the initial plume source relative to a fixed trailing-edge slab. Our experiments highlight the conditions under which the slab-induced poloidal and toroidal flows affect the plume dynamics and vice-versa. Natural cases of plumes in the vicinity of a subduction zone are finally discussed.

## 2. Analogue Modelling

We used a Perspex tank 1 m long, 0.62 m wide and 0.60 m deep that was filled with glucose syrup, a Newtonian fluid, up to  $H=0.45$  m. A plate of thickness  $d=0.015$  m, width  $W=0.20$  m, and length  $L=0.50$  or  $0.60$  m made of high-viscosity linear-viscous silicone (Wacker Silicone) mixed with fine iron powder was used to model an oceanic plate. The glucose syrup density was  $\rho_a = 1413$  kg/m<sup>3</sup>, and its viscosity  $\mu_a$  varied within the range 74-119 Pa s due to temperature variations. The plate density of 1513 kg/m<sup>3</sup> was larger than that of the glucose by  $\Delta\rho_s=100$  kg/m<sup>3</sup>. The plate dynamic shear viscosity  $\mu_s$  of 64,000 Pa s was substantially larger than the glucose syrup viscosity  $\mu_a$  as the ratio  $\gamma = \mu_s/\mu_a$  was within the range 538–865. The plate was fixed along its trailing edge to one of the lateral walls. Subduction of the plate was initiated by downward bending a length of its free edge  $l_{top}$  equivalent to 3 cm as measured from the top by an angle  $\theta_0$ . Black neutrally buoyant spheres to be used as slab-induced flow tracers were spread at the top surface. A compositional plume was introduced at the base of the tank through a nozzle. The plume fluid was made of glucose syrup diluted with water resulting in a plume density less than that of the glucose syrup by

87  $\Delta\rho_p=40\text{ kg/m}^3$ , and a viscosity  $\mu_p = 5\text{ Pa s}$ . The buoyant fluid was supplied  
 88 by a pressure vessel and was dyed to make the plume clearly visible. In each  
 89 experiment, we maintained a constant input volume flux  $Q$ . Figure 1 shows  
 90 the laboratory setup and the different initial plume positions. Photos were  
 91 taken every 10 seconds simultaneously from two sides, and from the top.

92 Lengths of the model were scaled so that 1 cm represents 50 km in nature.  
 93 The time was scaled by the time a slab element takes to sink through the  
 94 model depth  $H$  at the velocity scale  $\hat{U} = \Delta\rho_s g d^2 / \mu_a = \gamma \Delta\rho_s g d^2 / \mu_s$ , resulting  
 95 in

$$\frac{t^{Nature}}{t^{Model}} = \frac{H^{Nature}}{\hat{U}^{Nature}} \times \frac{\hat{U}^{Model}}{H^{Model}} = \left( \frac{H^{Nature}}{H^{Model}} \right) \left( \frac{(\gamma \Delta\rho_s g d^2 / \mu_s)^{Model}}{(\Delta\rho_s g d^2 / \mu_a)^{Nature}} \right), \quad (1)$$

96 where  $g$  is the gravitational acceleration. Hence one second typically repre-  
 97 sents about 7 kyr, using a model  $\gamma$ , a mantle depth  $H$  and mantle viscosity  
 98  $\mu_a$  of 640, 2000 km and  $10^{20}\text{ Pa s}$ , respectively. The presented models are  
 99 deep mantle models and no stratification of the mantle is considered. We  
 100 defined the slab buoyancy flux  $B_s$  by

$$B_s/g = \Delta\rho_s U W d, \quad (2)$$

101 where  $U$  is the slab steady sinking rate, while the plume buoyancy flux  $B_p$  is  
 102 given by

$$B_p/g = \Delta\rho_p Q, \quad (3)$$

103 (see also Appendix S1). In experiments 4-21, as well as the plume relative  
 104 position to the slab, we varied the buoyancy flux ratio  $B_s/B_p$ .

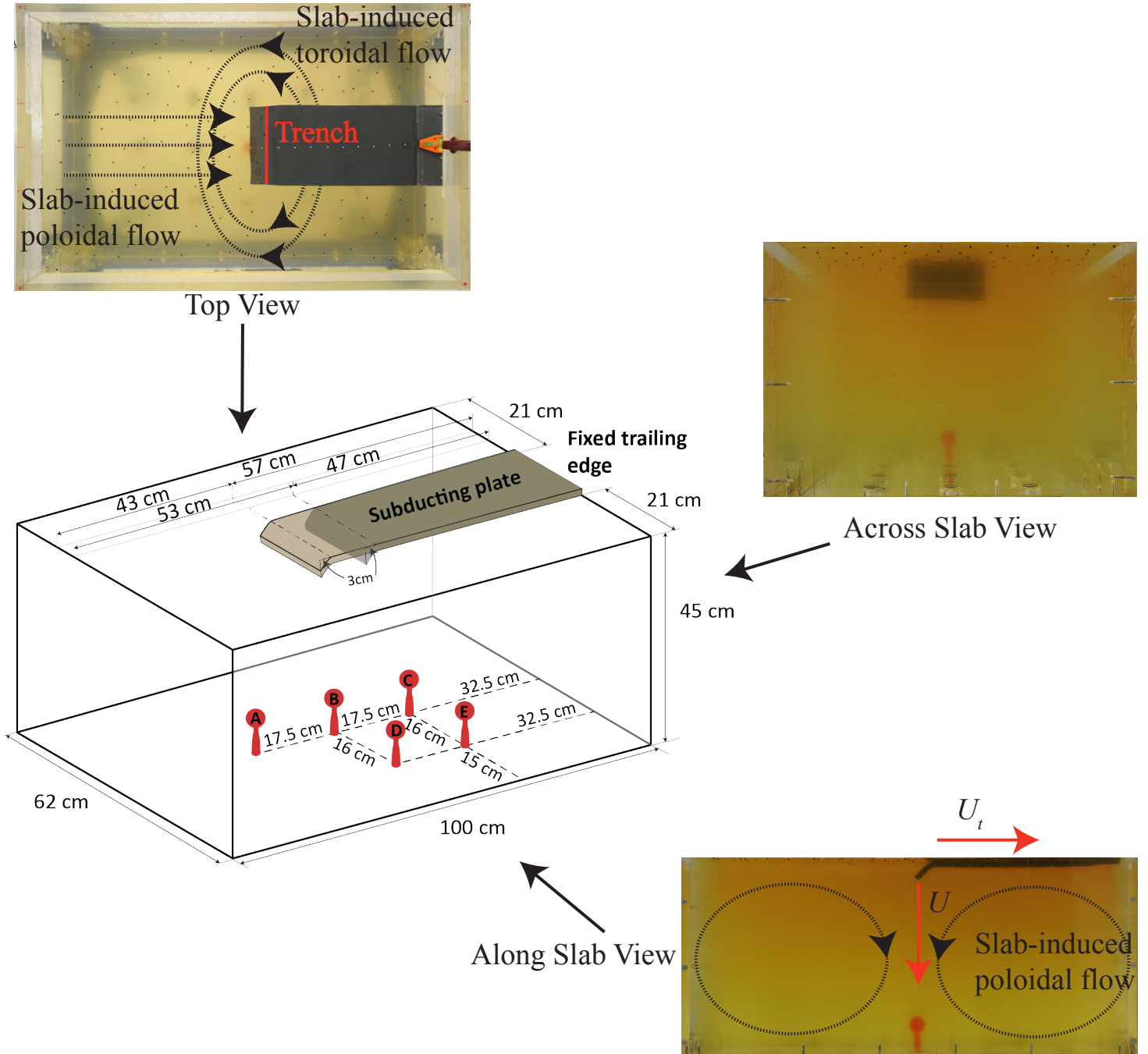


Figure 1: Experimental setting. The plume positions used for the experiments are shown and referred to in Table 1.

| <i>Experiments</i> |                 | $W$  | $d$  | $L$  | $\gamma$ | $\theta_0$ | $S_0$ | $U_0^*$ | $U$    | $U_{edge}$ | $B_s/g$   | $B_p/g$  | $B_s/B_p$ |
|--------------------|-----------------|------|------|------|----------|------------|-------|---------|--------|------------|-----------|----------|-----------|
|                    |                 | (cm) | (cm) | (cm) |          | (degrees)  |       | (cm/s)  | (cm/s) | (cm/s)     | (kg/s)    | (kg/s)   |           |
| Errors             |                 |      |      |      | 10%      | 3°         | 18%   | 7.6%    | 5%     | 5%         | 5%        | 5%       | 10%       |
| 1                  | Slab-only       | 20   | 1.5  | 50   | 610      | 11.9       | 4.02  | 0.43    | 0.0581 | 0.0487     | 1.452e-4  | 0        | $\infty$  |
| 2                  | Slab-only       | 20   | 1.5  | 50   | 566      | 19.1       | 3.53  | 0.41    | 0.0718 | 0.0613     | 2.153e-4  | 0        | $\infty$  |
| 3                  | Slab-only       | 20   | 1.5  | 60   | 836      | 14.5       | –     | 0.59    | 0.0910 | 0.0764     | 2.731e-4  | 0        | $\infty$  |
| 4                  | Front-plume (B) | 20   | 1.5  | 50   | 610      | 20.9       | 3.99  | 0.45    | 0.0579 | 0.0474     | 1.736e-4  | 1.739e-6 | 99.89     |
| 5                  | Front-plume (B) | 20   | 1.5  | 50   | 640      | 14.6       | 4.64  | 0.46    | 0.0569 | 0.0462     | 1.706e-4  | 4.322e-6 | 39.48     |
| 6                  | Front-plume (B) | 20   | 1.5  | 50   | 593      | 16.3       | 4.19  | 0.42    | 0.0625 | 0.0520     | 1.875e-4  | 7.164e-6 | 26.18     |
| 7                  | Front-plume (B) | 20   | 1.5  | 50   | 566      | 24.8       | 3.38  | 0.43    | 0.0739 | 0.0606     | 2.217e-4  | 1.405e-5 | 15.78     |
| 8                  | Front-plume (A) | 20   | 1.5  | 60   | 566      | 24.0       | 3.45  | 0.43    | 0.0708 | 0.0601     | 2.123e-4  | 1.422e-5 | 14.93     |
| 9                  | Front-plume (B) | 20   | 1.5  | 60   | 627      | 20.5       | 4.06  | 0.46    | 0.0589 | 0.0495     | 1.766e-4  | 1.413e-5 | 12.50     |
| 10                 | Rear-plume (C)  | 20   | 1.5  | 60   | 593      | 16.8       | 4.15  | 0.43    | 0.0634 | 0.0555     | 1.901e-4  | 7.569e-6 | 25.12     |
| 11                 | Rear-plume (C)  | 20   | 1.5  | 60   | 538      | 36.7       | 3.76  | 0.49    | 0.0725 | 0.0608     | 2.175e-4  | 1.755e-5 | 12.39     |
| 12                 | Rear-plume (C)  | 20   | 1.5  | 60   | 538      | 36.7       | 3.77  | 0.47    | 0.0720 | 0.0607     | 2.159e-4  | 3.264e-5 | 6.61      |
| 13                 | Rear-plume (C)  | 20   | 1.5  | 60   | 842      | 19.8       | –     | 0.61    | 0.1018 | 0.0876     | 3.054 e-4 | 7.424e-5 | 4.11      |
| 14                 | Rear-plume (C)  | 20   | 1.5  | 60   | 810      | 16.8       | –     | 0.58    | 0.0921 | 0.0797     | 2.764e-4  | 7.633e-5 | 3.62      |
| 15                 | Rear-plume (C)  | 20   | 1.5  | 60   | 842      | 17.2       | –     | 0.61    | 0.0910 | 0.0743     | 2.726e-4  | 7.854e-5 | 3.47      |
| 16                 | Rear-plume (C)  | 20   | 1.5  | 60   | 865      | 20.7       | –     | 0.64    | 0.0923 | 0.0735     | 2.769e-4  | 8.035e-5 | 3.44      |
| 17                 | Rear-plume (C)  | 20   | 1.5  | 60   | 780      | 22.6       | –     | 0.58    | 0.0891 | 0.0783     | 2.674e-4  | 9.109e-5 | 2.93      |
| 18                 | Rear-plume (C)  | 20   | 1.5  | 60   | 847      | 11.6       | –     | 0.60    | 0.0972 | 0.0837     | 2.864e-4  | 1.264e-4 | 2.26      |
| 19                 | Side-plume (E)  | 20   | 1.5  | 60   | 593      | 18.8       | 4.02  | 0.43    | 0.0611 | 0.0529     | 1.845e-4  | 7.086e-6 | 26.05     |
| 20                 | Side-plume (D)  | 20   | 1.5  | 60   | 566      | 26.8       | 3.22  | 0.44    | 0.0771 | 0.0647     | 2.312e-4  | 1.22e-5  | 19.07     |
| 21                 | Side-plume (E)  | 20   | 1.5  | 60   | 538      | 20.3       | 3.41  | 0.39    | 0.0704 | 0.0581     | 2.111e-4  | 1.297e-5 | 16.27     |

Table 1: Model dimensions (see also Appendix S1).

### 105 3. Results

106 We present experiments that include different initial positions of the  
107 plume relative to the slab and different buoyancy flux ratios  $B_s/B_p$ . We  
108 catalogued the relative plume positions into three classes: the front, rear and  
109 side plume positions, respectively (see Table 1 and Figure 1). The plume was  
110 initiated at a time  $t_p^i = 20$  s after subduction of the plate had been initiated,  
111 except for experiments 13, 15, 16 and 18, for which the plume was started  
112 at  $t_p^i = 610, 330, 700$ , and  $250$  s, respectively, after subduction initiation.

113 In all experiments, slabs first steepened with time (up to  $\sim 90$  degrees  
114 for the bottom half of the slab, and then steadily sunk and retreated while  
115 attaining a dip angle of  $\sim 50$  degrees (e.g. Figs. 2-4). Slabs were also seen  
116 to curl along their lateral edges in response to the drag of the surrounding  
117 mantle, producing a top-view curvature that is concave towards the mantle  
118 wedge. Finally, as the slab tip approached the bottom of the tank, slab  
119 rollback and slab sinking decelerated. This subduction process induces a flow  
120 in the mantle that can be decomposed into slab-induced toroidal and slab-  
121 induced poloidal components (see Strak and Schellart (2014) for stereoscopic  
122 Particle Image Velocimetry of slab-induced 3-D mantle flow). These two  
123 components vary in space and time as the slab lengthens. In particular,  
124 the slab-induced flow is characterized by the two poloidal circulations in the  
125 mantle wedge and sub-slab domain, and the two toroidal cells around the  
126 lateral slab edges (see Figure 1). In our experiments, the extent of the slab-  
127 induced poloidal and toroidal circulation at the surface were estimated as  
128 a function of slab length using the neutrally buoyant tracers that had been  
129 seeded at the surface (Appendix S2.1).

### 130 3.1. Generic Front, Rear and Side plume experiments 6, 10 & 19

131 We qualitatively detail here experiments 6, 10 & 19, which model three  
132 plume positions, front, rear and side, relative to the plate for a similar buoy-  
133 ancy flux ratio  $B_s/B_p = 25.78 \pm 0.58$ .

#### 134 3.1.1. Front plume experiment 6

135 The plume was initiated at the apex of the slab tip. It took about 200  
136 s for the plume head to grow and lift up from the bottom. The plume then  
137 rose vertically for about 250 s until it started to be deflected away from the  
138 slab due to the slab-induced poloidal circulation in the wedge. This deflec-  
139 tion continued until the plume head reached the height of the slab tip at a  
140 time of 670 s (Figure 2a, 2b & 2c). At this stage, the plume head was still  
141 fairly axisymmetric; the plume and slab tip were 9 cm apart. Beyond this  
142 time, the plume head and upper part of the conduit began to be increasingly  
143 advected towards the slab and trench by the poloidal circulation, and the  
144 plume head became elongated in the direction perpendicular to the trench  
145 (Figure 2d, 2e & 2f). During this late stage, the plume deformation also  
146 resulted from the mantle return flow due to the slab’s rollback motion dom-  
147 inated by the toroidal component. In particular, it resulted in the plume  
148 head being pinched at its end. A movie named Movie-Front-Plume showing  
149 the dynamics of the interaction over time is provided in the Appendix.

#### 150 3.1.2. Rear plume experiment 10

151 The plume was initiated underneath the slab 17.5 cm away from its tip.  
152 The plume rose vertically for 640 s. The influence of the slab started when  
153 the slab tip and the plume head reached the same vertical position. Due to

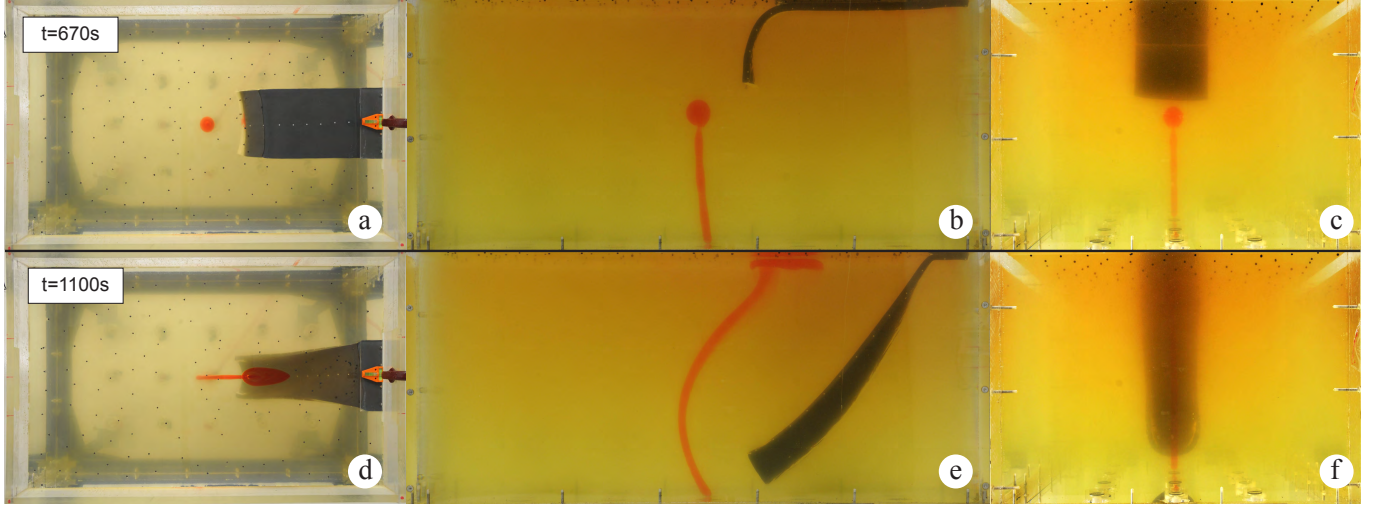


Figure 2: Two stages of the front-plume experiment 6 showing the slab/plume interaction at  $t=670$  s (top frames a, b and c) and 1100 s (bottom frames d, e and f). The three top and bottom frames represent the top, along (side) and across (front) slab views from left to right, respectively.

154 the slab-induced poloidal circulation, the plume head then began to develop  
 155 an asymmetry pulling down its left side, and the conduit got slightly bent  
 156 as shown in the Figure 3b. Thereafter, the plume got further swept away  
 157 by the slab during its rollback motion. Significant flattening of the plume in  
 158 the direction perpendicular to the slab plane (and elongation parallel to the  
 159 trench), including its head and its conduit, occurred during this phase due  
 160 to slab-induced toroidal flow, as is shown in Figure 3f. Ultimately, the whole  
 161 plume underplated the slab (this can be seen in the movie provided in the  
 162 Appendix named Movie-Rear-Plume).



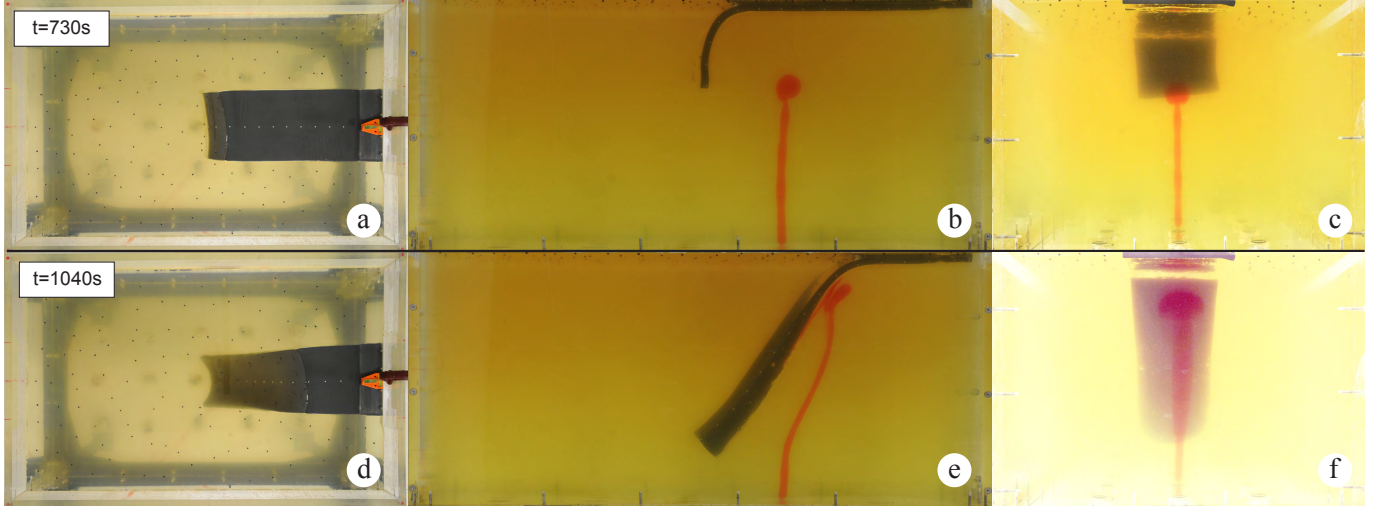


Figure 3: Two stages of Rear-plume experiment 10 showing the slab/plume interaction at  $t=730$  s (top frames a, b and c) and 1040 s (bottom frames d, e and f). The three top and bottom frames represent the top, along (side) and across (rear) slab views from left to right, respectively. We note that the color scheme in frame f was modified to enhance the plume visibility.

### 163 3.1.3. Side plume experiment 19

164 In experiment 19, the plume was initiated 17.5 cm at the rear of the  
 165 initial slab tip, and on the side of the slab 16 cm away from its centreline.  
 166 For 630 s, the plume rose while very slightly tilting by 1.1 degree towards  
 167 the slab as shown in Figure 4a, 4b & 4c. The plume head became very  
 168 slightly asymmetric. At this stage, the slab tip and the plume head had not  
 169 yet reached the same vertical position. As the trench arrived in the vertical  
 170 plane of the plume, the latter started a clockwise rotation under the influence  
 171 of the slab-induced toroidal flow, before being further dragged towards the  
 172 trench by the slab-induced poloidal flow in the mantle wedge, as shown in  
 173 Figure 4d, 4e & 4f. This process occurred in about 460 s, scaling to 3 Myr.

174 A movie named Movie-Side-Plume is included in the Appendix.

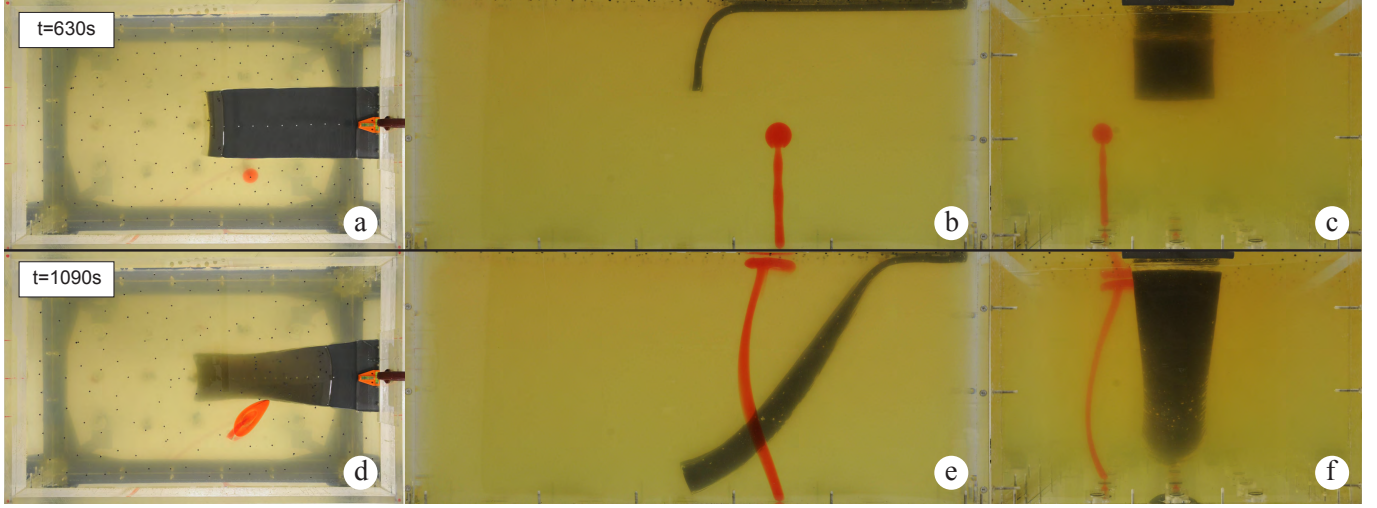


Figure 4: Two stages of the Side-plume experiment 19 showing the slab/plume interaction at  $t=630$  s (top frames a, b and c) and 1090 s (bottom frames d, e and f). The three top and bottom frames represent the top, along (side) and across (rear) slab views from left to right, respectively.

### 175 3.2. Slab sinking rates

176 As the plate is not motor-driven but left to sink on its own, the slab  
 177 sinking rate is not *a priori* known and requires an *a posteriori* analysis.  
 178 We used the side-view photos to analyze the tip position with time. An  
 179 initial transient phase that will be further discussed in section 3.3.1 is seen  
 180 across all experiments. This phase, whose sinking regime is in a stiffness  
 181 dominated regime (see Appendix S2.2), slightly varies between experiments  
 182 due to unavoidable slight differences in the tip initiation. However, beyond  
 183 this phase all experiments exhibit a steady linear sinking rate of the tip  $U$ ,  
 184 until the tip approaches the bottom of the tank. The slab steady sinking rate

185 was determined by linear fits on the slab tip positions as a function of time in  
 186 the interval between the initial transient, typically after 500 s, and before the  
 187 slab deceleration as it approached the bottom. As the plate was subjected  
 188 to some transverse deformation during its sinking, we measured the sinking  
 189 speed of the slab's at its centre  $U$  and at its lateral edge  $U_{edge}$ . The middle  
 190 of the slab systematically sunk faster than its sides with  $U$  being larger than  
 191  $U_{edge}$  by 10% to 19% (Table 1). These results are consistent with those of Li  
 192 and Ribe (2012) whose difference in sinking speeds was up to 20%.

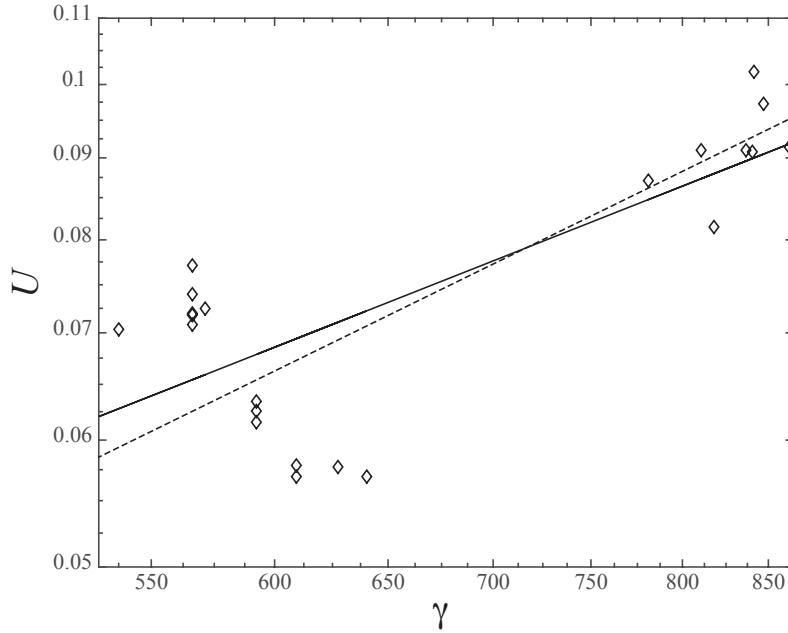


Figure 5: The slab tip sinking rates. Log-log plot of sinking speeds  $U$  as a function of  $\gamma = \mu_s/\mu_a$ . The straight black line is the fit obtained for all experiments by linear regression, whose slope is 0.80 and root mean squared error is 0.13. The dashed black line is the fit obtained for experiment 3, 6, 10 & 13-19 by linear regression, whose slope is 0.99 and root mean squared error is 0.05.

Figure 5 shows the steady sinking rates  $U$  as a function of  $\gamma$  on a log-log scale for all experiments. We find that there is a general trend for a decrease of the velocity as  $\gamma$  increases. The slope of the fit obtained by linear regression is not strictly 1, as expected in the Stokes regime, but 0.8 with a root mean squared error of 13.5%. However, if we consider experiments 3, 6, 10 & 13-19 only, the sinking velocity  $U$  appears to vary more convincingly as  $\mu_a^{-1}$ , equivalently  $\gamma$ , as the fit obtained by linear regression has a slope of 0.99 with a root mean squared error of 0.05. We note that a similar fit by linear regression for the experiments 1-2, 4-5, 7-9, 11-12 & 20-21 does not give a slope of 1 but -2. In part, this can be attributed to the errors made in measuring the viscosity of order 5%, but this is not sufficient to explain some apparent errors of the viscosity of 12-24% for experiments 1-2, 4-5, 7-9, 11-12 & 20-21. So it seems that, for the latter experiments, the sinking rate variations would not be explained by the viscosity variations alone. Some influence of the initial conditions cannot be excluded. Based on dimensional analysis, Li and Ribe (2012) for example predicted that  $U$  would be a function of  $\theta_0$ , even though such a dependency is not perceived through our values of  $U$  and  $\theta_0$ .

### 3.3. Impact of buoyancy flux ratio and plume positioning

#### 3.3.1. Plume influence on slab subduction

The previous sinking rate analyses were performed regardless of the buoyancy flux ratio  $B_s/B_p$ . In other words, the changes in sinking rates were not attributed to plume buoyancy but rather to viscosity and, to a lesser degree, initial conditions variations. For instance, the sinking rates of the slab in the front, rear and side plume experiments 6, 10 & 19 and slab-only experiment

218 1, which had a similar initial plate stiffness  $S_0 = 4.06 \pm 0.13$  (Appendix S2.2,  
 219 equation 2), and a similar buoyancy ratio  $B_s/B_p = 25.78 \pm 0.58$ , when in  
 220 the presence of a plume, differed by only 4% although the initial transients  
 221 occurred over varying time intervals from 610 s to 760 s (i.e. a time difference  
 222  $\delta t_i = 150$  s), times at which the slab had typically reached 12 cm (600 km)  
 223 (Figure 6a). Similarly, experiments 2, 7, 8, 11 & 21 of buoyancy flux ratio  
 224  $B_s/B_p = 14.84 \pm 1.72$  and  $S_0 = 3.51 \pm 0.15$ , and whose transients time vary-  
 225 ing from 490 to 640 s had a similar  $\delta t_i = 150$  s and similar slab lengths of  $\approx$   
 226 12 cm, had sinking rates that differed by no more than 2% (Appendix Figure  
 227 S2.2). At those buoyancy flux ratios, there was thus no plume influence on  
 228 the slab to be found.

229 By contrast, at lower buoyancy ratios  $B_s/B_p \sim 3$  (experiments 13-16  
 230 & 18), although the sinking rates were all consistent, the initial transient  
 231 phase showed a lot more variability as shown in Figure 6b. The extent of  
 232 such variability cannot be explained by differences in the initiation alone. In  
 233 particular, experiment 14 did not start to sink at a steady rate before 830 s,  
 234 a transient time 1.4 times longer than the transient time of experiments 3,  
 235 13, & 16, spanning a time interval of 520 – 670 s, at which slabs were all  $\approx 12$   
 236 cm long. In fact, over much of its transient, the plate was subjected to the  
 237 force of a strong plume that started to spread axisymmetrically underneath  
 238 the plate while the slab was only 4 cm long. The plume thus postponed  
 239 the subduction process for at least 150 s ( $\sim 1.3$  Ma). In experiment 18, the  
 240 strong plume did postpone subduction for only  $\approx 50$  s because it afterwards  
 241 started to underlie the slab, as the latter was already 8 cm long, hence close  
 242 to the 12 cm threshold for steady sinking. The transient phase of experiment

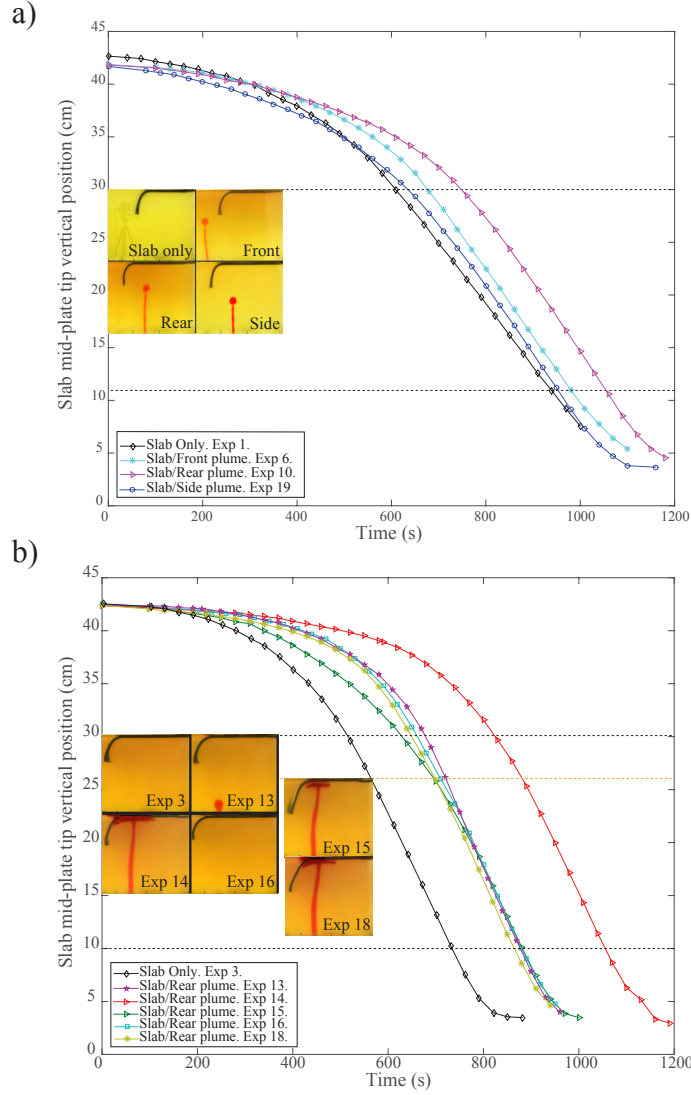


Figure 6: Slab tip vertical positions as a function of time. a) Slab only experiment 1 and, slab and Front, Rear and Side plume experiments 6, 10 & 19, respectively. b) Slab only experiment 3 and, slab and Rear plume experiments 13-16 & 18, respectively. The two black dashed lines indicate the two vertical positions between which linear regressions on the slab tip positions were made to determine the slab steady sinking rates  $U$  given in Table 1. For experiments 15 and 18, the linear regression started at a greater depth (at the level of the orange dashed line). The ten inserts show the slab and plume positions from where the linear regressions start. 17

15 was also peculiar. It lasted 700 s while a strong plume underlay the plate from a time of 610 s, where the slab was 12 cm long ready to begin its steady sinking phase. The plume halted it for 90 s ( $\sim 0.8$  Ma). Interestingly, the plume initial impact in experiment 15 was closer to the plate bend at 12 cm compared to 20 cm away in experiments 14 and 18. Plumes in experiments 14, 15 & 18 thus interfere with the plate bending as they represent a sufficient net vertical shear force

$$F_p = \Delta\rho_p(Q/A_p)^2, \quad (4)$$

where  $A_p$  is the area of the plume underneath the plate, opposing the vertical traction due to the plate negative buoyancy,

$$F_b = \Delta\rho_s g d l W. \quad (5)$$

Estimates of  $F_p$  and  $F_b$  at the time of plume spreading initiation underneath the plate show that  $F_p/F_b$  ratios were 29%, 22% and 21% for experiments 14, 15 & 18 respectively (see Appendix Table S2.2). Note that  $F_p/F_b$  ratios are consistent with experiment 14 having the most plume influence on bending. Although involving strong plumes, experiments 13 & 16 did not show a modified subduction because plumes interacted with slabs of increasing lengths, and hence of greater  $F_b$ . In particular, these strong plumes did not modify the slab's dip angle. This work modelling subduction in a whole mantle contrasts with that of recent upper-mantle models (Mériaux et al, 2015b) for which  $F_b$  was limited by the model depth. Nevertheless subduction can be slowed down in both cases, during the bending phase in the first case, and during the steady retreat in the second case. Furthermore, in these experiments, strong plumes could spread axisymmetrically underneath the plate as

the slab was initiated, but then preferentially spread towards the trench as the slab-induced poloidal flow established itself (see also the supplementary information, Mériaux et al, 2015b).

### 3.3.2. *Plume head asymmetry & flattening*

In all experiments, plume head asymmetry develops. Front plumes were elongated in the trench-normal direction by the slab-induced poloidal flow component in the mantle wedge, side plumes were elongated in a direction oblique to the trench axis by the slab-induced mixed poloidal and toroidal flow components in the sub-slab/mantle wedge transition region (see Figures 2 & 4). Rear plumes were elongated in the trench-parallel direction due to flattening in the trench-normal direction by the slab-induced toroidal flow component (see Figure 3), unless they had reached the surface before the slab had lengthened enough to generate efficient toroidal flow. This happened in experiments 14, 15, 17 & 18, which had a high buoyancy plume relative to the slab, but not experiments 13 and 16 because of the delay in plume initiation. Figure 7 shows that trench-normal flattening started as the slab-induced toroidal flow component could influence the plume, which occurs when the plume and the slab reach the same height, highlighted by arrows in Figure 7. The amount of flattening linearly increased with the retreat rate, and hence the magnitude of the slab-induced toroidal flow component.

Once underneath the slab, on-going flattening of rear plumes actually led to increased plume volume as the plume buoyancy increased. In experiments 10, 11, 12 and 18, sorted by increase buoyancy, the surface area of plume fluid underneath the slab was 39%, 56%, 79% and 87% that of the slab, respectively, at the end of each experiment. So the slab is eventually



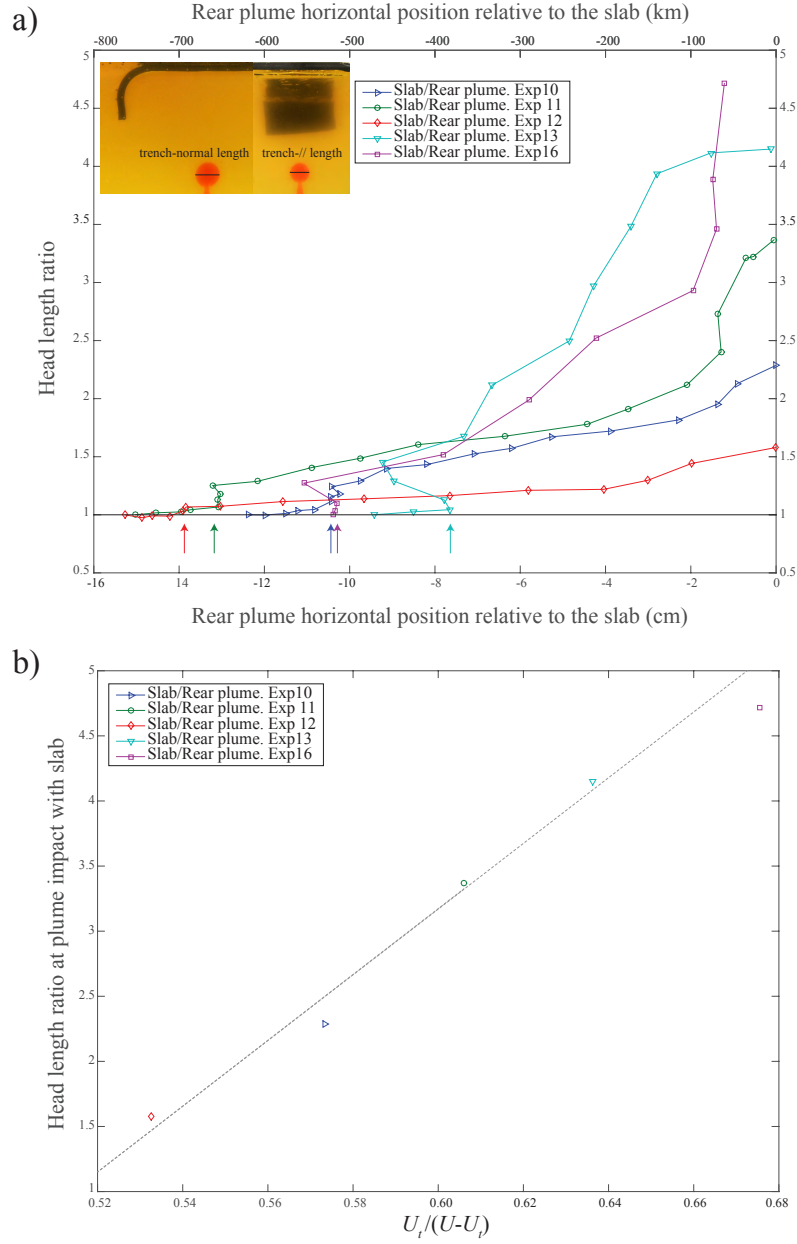


Figure 7: a) Ratio of the trench-parallel (from rear view) by the trench normal (from along view) lengths of the plume head as a function of distance between the slab and the plume measured at plume head mid-height for rear plume experiments 10-13 & 16. Each arrow indicates the distance at which the plume reached the slab depth. b) Ratio of the trench-parallel (from rear view) by the trench-normal lengths of the plume head when the slab reaches the plume as a function of dimensionless retreat rate  $U_t/(U-U_t)$  with  $U_t < 0$ . The black dashed line shows the linear fit.

almost underlain by a fluid of lesser density and viscosity. Interestingly, the slab sinking rate is not seen to be sensitive to such a lesser viscous layer or “ambient” as the sinking rate is not seen to increase.

### 3.3.3. *Tilt initiation & Maximum tilt*

The slab/plume interaction can take place even when slab and plume are far apart. This is especially true for front plumes which are sensitive to the slab-induced downwelling associated with the poloidal circulation in the mantle wedge. In experiments 4, 5, 6 & 7, due to such downwelling, plumes started tilting towards the mantle wedge at increasing depths as the slab/plume buoyancy ratio was increased. Plumes thus reached a tilt of three degrees (equivalent to a horizontal displacement of 2.36 cm or 118 km over a depth of 45 cm or 2250 km, respectively) at a distance from the slab tip of 5 cm (250 km), 11 cm (550 km), 18 cm (900 km), and 27 cm (1350 km) as the slab/plume buoyancy flux ratios of experiments 4, 5, 6 & 7 increased from 16 to 26, 39 & 100, respectively (see Appendix S2.5).

In contrast, for the side and rear plume positions, tilting of the plume began when plume and slab were at about similar depths regardless of  $B_s/B_p$ . During the experiments, the plume tilt varied in time and space, and could be substantial as for experiment 8, which exhibited a plume conduit tilted by as much as  $66^\circ$  (Appendix Figure S2.4).

### 3.3.4. *Plume material capture in the mantle wedge*

In a retreating subduction mode, regardless of the initial plume position, the slab-induced toroidal flow is very efficient at capturing plume material in the mantle wedge as shown in Figure 8. In experiments 8, 9, 18 & 21,

314 plume material even started to be subducted towards the end of slab retreat.  
315 In experiment 18 (Figure 8), the slab at the end of the experiment was also  
316 wrapped at depths by plume material, down to about 28 cm (1400 km).  
317 Front plumes that are of lesser buoyancy and under a greater influence of the  
318 combined slab-induced poloidal and toroidal flow due to their proximity to  
319 the slab during their ascent (e.g., in experiment 8, at its arrival at the surface,  
320 the plume is  $\sim 9$  cm (450 km) apart from the trench) can be entirely dragged  
321 towards the trench along a line (Figure 8, top left frame). By contrast, plumes  
322 of higher buoyancy and further away from the trench (e.g. in experiment 9,  
323 at its arrival at the surface,  $\sim 16$  cm (800 km) separates the plume and the  
324 trench) can keep memory of the purely axisymmetric spreading in the limit  
325 of no-ambient shear or infinitely buoyant plumes (Figure 8, top right frame).

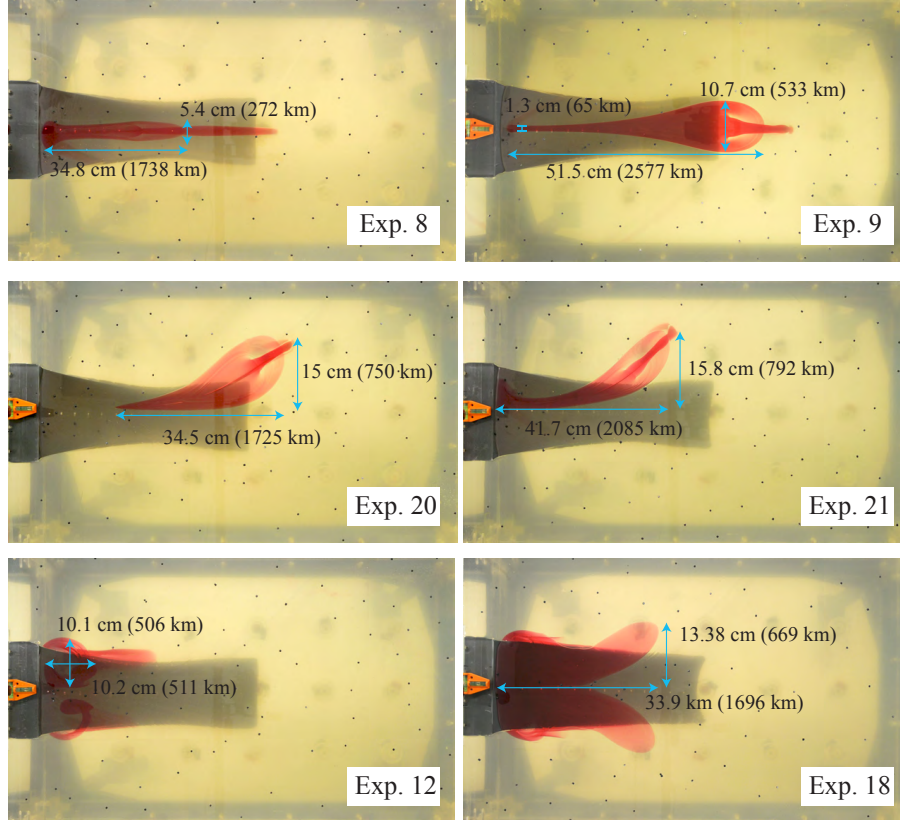


Figure 8: Plume material distribution after interaction with a retreating slab. Top frames are front plume experiments 8 & 9, from left to right, respectively. Middle frames are side plume experiments 20 & 21, from left to right, respectively. Bottom frames are rear plume experiments 12 & 18, from left to right, respectively. The blue arrows indicate the horizontal extent of plume material at the surface. The plume lateral spreading at the surface is influenced by both the slab-induced poloidal and toroidal flow components. This shows that the spatial distribution of mixed plume-arc-related magmatism could actually be extremely variable, and depending on the plume position relative to the slab, could be found from along a line to within a pear shape region or torus in the mantle wedge.

### 326 3.3.5. Sensitivity of slab/plume relative position

327 Varying the proximity between plume and slab within the same region  
328 can have its importance. This is best shown by experiments 7 & 8. These two  
329 front plume experiments differed by only 5% in  $B_s/B_p$  but differed by their  
330 plate lengths of 50 and 60 cm, respectively. The subsequent slightly different  
331 initial position of the plume relative to the slab (Appendix Figure S2.5)  
332 later resulted in a closer proximity of the plume and the slab. In addition,  
333 compared to experiment 7, the plume in experiment 8 rose at a slower rate  
334 as shown in Figure S2.5 due to a much greater influence of the slab-induced  
335 downwelling associated with the poloidal circulation in the mantle wedge.

## 336 4. Discussion

### 337 4.1. Application to nature

338 The range of plausible slab/plume buoyancy flux ratios  $B_s/B_p$  in nature  
339 today is 0.2–710 (see Appendix Table S3.1). Apart from its lowest and high-  
340 est bounds, our experiments are within a range of 2-100, which overlaps the  
341 range in nature. The dynamics of subduction systems on Earth is commonly  
342 classified into three modes that differentiate by their absolute motion of the  
343 trench: a retreating mode, an advancing mode, and a quasi-stationary mode  
344 (Schellart et al., 2008). In effect, these three modes differ in their partition-  
345 ing of the poloidal and toroidal flows. Plume deflection being a response to  
346 the poloidal and toroidal flows will thus differ across the different subduction  
347 modes. However, the retreating mode is the most frequent mode (Schellart  
348 et al., 2008). Long-term trench advance and slab roll-forward appear non-  
349 existent on Earth as slab roll-over geometries do not exist on Earth (Ribe,

2010). In our experiments, we model a retreating mode that generates significant toroidal mantle flow providing a mechanism for mantle plume material to be dragged towards the mantle wedge. By contrast, a quasi-stationary subduction mode will be dominated by the poloidal circulation that keeps the plume material in its original domain due to the absence of mass flux between the sub-slab and wedge regions (Figure 2; Kincaid and Griffiths, 2003). Our experiments also model a deep mantle, so the poloidal circulation is important. *Sensu stricto*, our experiments thus apply to slabs that would pass through the 670 km discontinuity. Systems with shallow slabs would retain a similar dynamics as that of whole mantle systems but with enhanced toroidal flows due to the viscosity interface (Royden and Husson, 2006).

#### 4.2. Modern plumes in the vicinity of subduction zones

As of today, there are a number of plumes among the catalogues of Sleep (1990), Montelli et al. (2006), Courtillot et al. (2003) in proximity of a subduction zone. If such proximity is a necessary condition for interaction, it is certainly not sufficient. Each potential system thus needs to be discussed on a case-by-case basis. Some systems have already been shown to bring together all the conditions for interaction. These are Cascadia/Yellowstone over the last 30 Myr (Kincaid et al., 2013), Tonga/Samoa (Druken et al., 2014), Gibraltar/Canary (Mériaux et al., 2015a), and Manila/Hainan (Mériaux et al., 2015b), and we refer to these publications for a detailed discussion of these systems. We describe below the case of four Pacific hotspots in the vicinity of a subduction zone (Figure 9).

In the Northeastern Pacific, the Bowie hotspot is part of the 900 km-

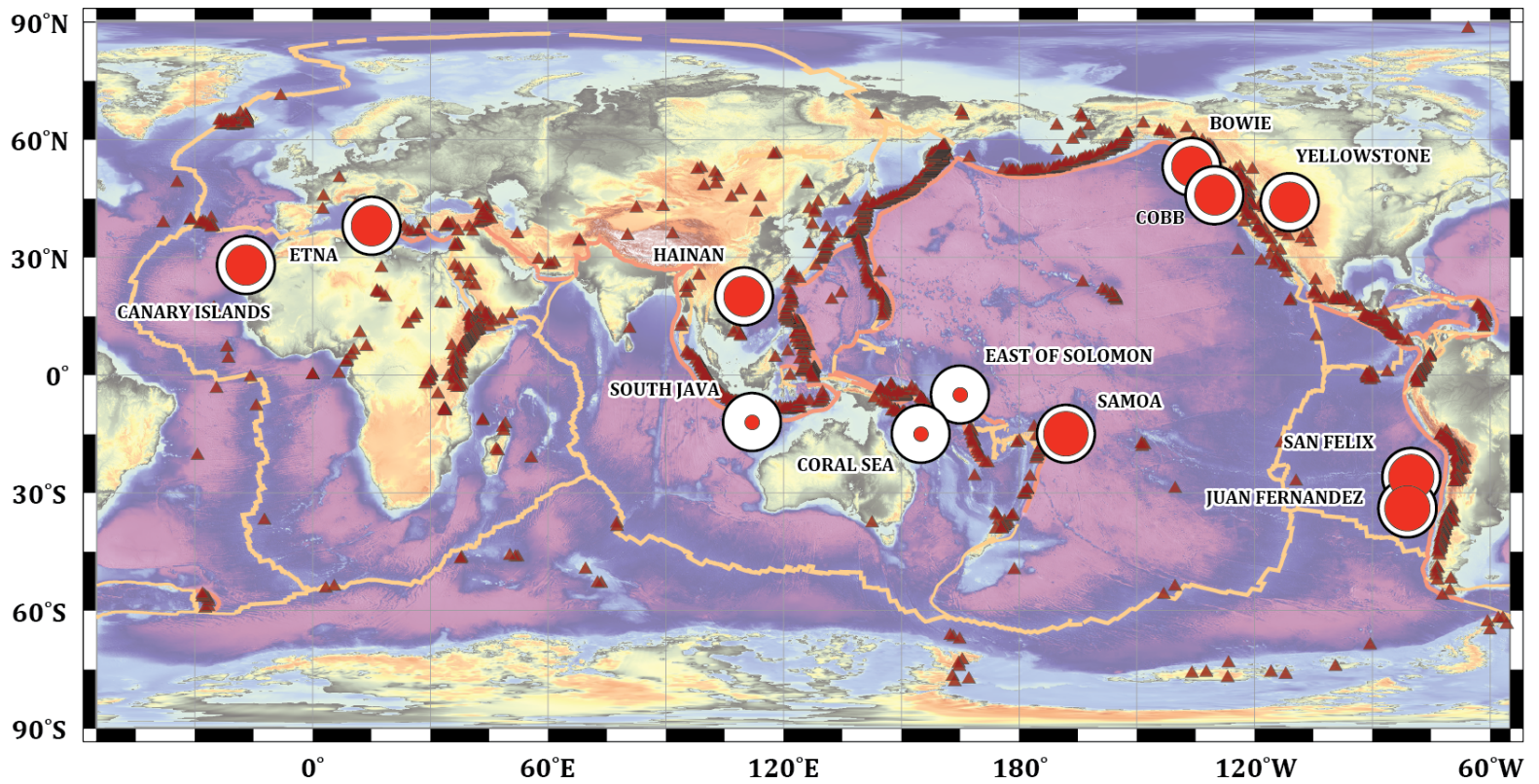


Figure 9: Selected modern plumes close to a subduction zone, either recently studied or discussed in this paper. Mantle plumes that do not reach the surface (white circles) are distinguished from those seen at the surface (red circles).

375 long Kodiak-Bowie seamount chain. The ages of the seamounts are typically  
 376 younger at Bowie ( $\geq 0.7$  Ma) than at Kodiak (up to 24 Ma) and essentially  
 377 reflect movement of the Pacific plate over the Bowie hotspot (Chaytor et al.,  
 378 2007). Parallel to this chain, the Cobb seamount chain extends from the  
 379 current location of the Cobb hotspot on the Juan de Fuca ridge to the 26  
 380 Ma Marchand Seamount, just oceanward of the Aleutian trench (Chaytor et  
 381 al., 2007). Both chains could well be older than  $\sim 20$  Ma as seamounts at  
 382 the termination of those tracks may have disappeared with the subduction  
 383 of the Pacific plate beneath Alaska over the last 60 Ma (Von Huene et al.,  
 384 2012; Heuret and Lallemand, 2005). Today Bowie is about 160 km west of  
 385 the Queen Charlotte transform Fault, a fault activated 30 Ma ago, and 320  
 386 km northeast of the northern termination of the Cascadia subduction zone,  
 387 from where the Juan de Fuca ridge sinks under the North American plate  
 388 (see Appendix Figure S3.1). The Cascadia subduction where the Juan de  
 389 Fuca plate, a remnant of the Farallon plate, is shoved underneath the North  
 390 American plate is today characterized by a southwestward trench retreat of  
 391 about 2.2-3.1 cm/yr for a convergence rate of the slab of about 4.4 cm/yr  
 392 (Schellart et al., 2011). In effect, Bowie could be considered in a side/rear  
 393 position relative to the retreating Cascadia trench (equivalent, in the lab-  
 394 oratory, to a position 6 cm from the plate edge and 2.7 cm at the rear of  
 395 the trench parallel direction and a buoyancy flux ratio of about  $\sim 5$ , see Ap-  
 396 pendix Table S3.2). Yet, despite such proximity and buoyancy flux ratio,  
 397 a present-day interaction is unlikely because Bowie and the Cascadia sub-  
 398 duction are disconnected by an active mid-oceanic ridge, the Juan de Fuca  
 399 Ridge, whose spreading is occurring at a half-rate of about 2.9 cm/yr (5.8



400 cm/yr total), in the direction parallel to the WNW-ESE fracture zones (e.g.  
 401 Atwater, 1970). Today the Bowie plume material is thus more likely to be  
 402 either entirely deflected away from the ridge by the Pacific plate flow or di-  
 403 vide itself into one part migrating toward the ridge and the other part being  
 404 deflected away from the ridge (Kincaid et al., 1995). Similarly, despite of its  
 405 close position ( $\sim 330$  km) at the rear of the Juan de Fuca retreating slab  
 406 and buoyancy flux ratio of  $\sim 10$  (Appendix Figure S3.1 and Table S3.2), the  
 407 Cobb hotspot has been under mid-oceanic ridges over the last 45 Ma, which  
 408 excludes the possibility of slab/plume interaction during this period (see the  
 409 movie PlateKinematic-HS-since60Ma.m4v provided in the Appendix).

410 In the Southeastern Pacific, the San Felix and Juan Fernández hotspots,  
 411  $\sim 930$  km apart, are located 820 and 835 km, respectively, west of or at the  
 412 rear of the shallow South-American subduction zone (Figure 9 and Appendix  
 413 Figure S3.2). Compared to Bowie and Cobb hotspots characterized by a  
 414 buoyancy flux of 600 kg/s and 300 kg/s, respectively, San Felix and Juan  
 415 Fernández are stronger hotspots with buoyancy fluxes estimated at 1600-2300  
 416 kg/s, and 1600-1700 kg/s, by Sleep (1990) and Davies (1988), respectively.  
 417 These plumes could be considered at the rear of a continuous 6000 km-  
 418 wide Nazca plate subducting at a rate of  $\sim 7$  cm/yr beneath the South  
 419 America plate with a retreat rate representing  $\sim 10$  to 25% of the subduction  
 420 velocity (Schellart et al., 2011), and a shallow depth of the slab (between 140  
 421 and 600 km). In this way, the Nazca/San Felix and Nazca/Juan Fernández  
 422 systems would be characterized by a similar buoyancy flux ratio  $B_s/B_p$  of  $\sim$   
 423 17 (Appendix Table S3.2), suggesting a slab dominated interaction.

424 With very limited mass flux between the sub-slab and wedge regions

425 following the quasi-stationarity of the trench, this subduction is to favour the  
426 poloidal flow in the sub-slab region, and consequently the tilting the plume  
427 towards the trench in the upper mantle some distance away from the trench,  
428 Additionally, regardless of retreat rates, the slab is in places very shallow,  
429 which does not promote slab-induced toroidal flow. In our experiments,  
430 short slabs do not generate toroidal flow that can be detected either from  
431 plume deflection or from the buoyant tracers displacement (Appendix S2.1).  
432 The limited slab-induced toroidal flow in the upper mantle actually appears  
433 consistent with the global tomography models showing a deflection of both  
434 plumes towards the east in the upper mantle rather than the west (Zhao,  
435 2007; Pesicek et al., 2012).

436 Now, whether the Andean slab is assumed continuous for  $\sim 6000$  km or  
437 segmented by slab windows and tears (Russo and Silver, 1994; Thorkelson et  
438 al., 2011), as currently debated, could lead to a different interaction with the  
439 San Felix and Juan Fernández plumes. Today, the Juan Fernández hotspot  
440 is aligned with the Juan Fernández ridge that is subducting obliquely under  
441 South America and likely causes the flattening of the slab as observed for  
442 the Nazca ridge further north. As to the young  $\sim 3$  Ma San Felix hotspot  
443 (Clouard and Bonneville, 2005), it is located between the Nazca and Iquique  
444 south migrating fossil ridges (Figure S2). In addition, while San Felix faces  
445 the well-developed 910-km wide slab of the hinge of the Andean Orocline,  
446 imaged by earthquakes to great depths (up to  $\sim 600$  km, Figure S2), Juan  
447 Fernández is at the rear edge of a much shallower ( $\sim 140$  km deep) and wider  
448 (2940 km) slab segment adjacent to a flat slab segment to the north. Inte-  
449 grating such segmentation would change the buoyancy flux ratios of the San

450 Felix/Nazca and Juan Fernandez/Nazca to  $B_s/B_p \sim 3$  and 10, respectively  
 451 (Appendix Table S3.2), and increase the roles of these plumes. In such a  
 452 geodynamic context, breaches of the Nazca slab in the region might develop  
 453 offering a direct path for the transfer of plume material to the mantle wedge,  
 454 similarly to the ridge-plume-slab scenario modelled by Betts et al. (2015)  
 455 but with a more complex slab geometry. Furthermore, even if, in the first  
 456 instance, the slab would keep its integrity and accommodate the deformation  
 457 by flexure alone, sub-slab grooves would develop and host plume channel  
 458 flows that would promote mechanical erosion, and possibly, the segmentation  
 459 of the South American slab. In other words, the oblique convergence of fossil  
 460 ridges together with the Pacific plumes of San Felix and Juan Fernández  
 461 could lead to the tearing of the Nazca slab and hence a significant mantle  
 462 flow reorganization in the southern Pacific.

#### 463 *4.3. Some implications*

##### 464 *4.3.1. Long-range interaction*

465 Our retreating slab mode experiments demonstrate that the slab/plume  
 466 interaction operates at long-range. Thanks to the poloidal circulation, plume  
 467 material can be captured at a distance of 885 km from the trench (Front  
 468 plume Exp. 9) and then dragged in the mantle wedge over 2700 km towards  
 469 the trench (Front plume Exp 9; Figure 8). Also, as discussed in section  
 470 3.3.3, whereas side and rear plumes would start being deflected when plume  
 471 and slab are at about similar depths regardless of buoyancy flux ratio, front  
 472 plumes could be tilted at great depths by slab-induced downwellings, the  
 473 depth of influence increasing with the plume “weakness”. This behaviour is  
 474 especially expected for the starting plume that is only visible in the lowermost

mantle up to 1900 km depth beneath the region East of Solomon (Montelli et al., 2006). Although the plume buoyancy is unknown, and the central San Cristobal segment is nearly stationary, a northeast tilt could be expected in the lower mantle due to slab downwelling. In contrast, the starting plume South of Java (seen up to 1450 km depth) (Montelli et al., 2006) being at the rear of the retreating Java subduction segment at  $\sim 2$  cm/yr southward should be less influenced at depths by the slab downwelling given the shallow slab depth. Provided that this subduction zone is stable, the interaction with this plume will start when the slab and plume reach similar depths. The starting plume in the Coral sea (seen up to 550 km depth) (Montelli et al., 2006), being at the rear of both retreating New Hebrides (slab depth  $\sim 400$  km) and New Britain (slab depth  $\sim 600$  km) subductions, at rates of  $\sim 4$ -5 cm/yr westward and southeastward, respectively (Schellart et al., 2011), would reflect such an interaction initiation. The long-range character of slab/plume interaction, both at depth, and at the surface, also implies that coeval plume and arc magmatism could be linked while being spatially separated, as shown by Heron et al. (2015) linking the large igneous province positions with paleosubductions over the last 300 Ma.

#### 4.3.2. *Plume-arc magmatic regions*

A variety of slab/plume interactions have been inferred from the presence of simultaneously arc-related and plume-related magmatism and contrasting geochemical signatures (see Appendix Table S3.3). While modern examples can benefit from the insights of tomography, past examples have been relying on additional plate reconstructions only. Our experiments suggest that the spatial distribution of mixed plume-arc-related magmatism could actually be

500 extremely variable in the event of an interaction (see Figure 8 in a rollback  
 501 subduction mode). Still our study provides for retreating slabs three clues to  
 502 corroborate slab/plume interaction. First, a plume at a rear of a subduction  
 503 zone or close to the lateral edge of a retreating slab can emerge in the mantle  
 504 wedge, and thus imprint the magmatic arc. Second, plumes at the front of  
 505 the subduction zone can be captured by the efficient poloidal flow at long  
 506 range distances (up to 2500 km), and similarly mix with the arc volcanism.  
 507 The third clue is the lateral plume spreading in the mantle wedge: The larger  
 508 the plume buoyancy flux, the more trench-parallel plume spreading, whereas  
 509 the closer the plume to the trench, the less trench-parallel plume spreading.

## 510 **5. Conclusion**

511 In this study, we have shown that slab/plume interaction is far from being  
 512 trivial but can develop into many scenarios. First, buoyant plume material  
 513 can underlie a slab over much of its area after slab/rear plume impact follow-  
 514 ing flattening of the plume in the trench-parallel direction during slab retreat.  
 515 Second, weak plumes can potentially be tilted at great depths when under  
 516 the influence of a slab downwelling in the mantle wedge. Third, plume mate-  
 517 rial can be captured at long-range distances, which can lead to a diversity of  
 518 potential plume source material distributions in the mantle wedge that will  
 519 ultimately be superimposed with arc magmatism. Last but not least, rear  
 520 plumes of sufficient buoyancy flux can halt subduction in the upper mantle.  
 521 Today there is no record of such event, but in the Archean period, during  
 522 which mantle plumes are thought to have been very strong, such a scenario  
 523 cannot not be ruled out, and it remains to be seen what the additional upper

524 mantle stratification would do in such a case. We hope that our study will  
525 prompt more systematic investigations of the interaction.

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## 675 S1. Appendix Supplementary Material: Slab/Plume system

### 676 S1.1. Model parameters

|  | Variable                         | Units                      |
|--|----------------------------------|----------------------------|
| <b><u>Ambient Fluid</u></b>            |                                  |                            |
| Gravitational acceleration             | $g$                              | $\text{m s}^{-2}$          |
| Ambient fluid density                  | $\rho_a$                         | $\text{kg m}^{-3}$         |
| Ambient fluid viscosity                | $\mu_a$                          | $\text{Pa s}$              |
| Ambient fluid depth                    | $H$                              | $\text{m}$                 |
| <b><u>Plate</u></b>                    |                                  |                            |
| Plate density                          | $\rho_s$                         | $\text{kg m}^{-3}$         |
| Plate density contrast                 | $\Delta\rho_s = \rho_s - \rho_a$ | $\text{kg m}^{-3}$         |
| Plate viscosity                        | $\mu_s$                          | $\text{Pa s}$              |
| Plate length                           | $L$                              | $\text{cm}$                |
| Plate width                            | $W$                              | $\text{cm}$                |
| Plate thickness                        | $d$                              | $\text{cm}$                |
| Slab length                            | $l$                              | $\text{cm}$                |
| Plate velocity                         | $U$                              | $\text{cm s}^{-1}$         |
| <b><u>Plume</u></b>                    |                                  |                            |
| Plume density                          | $\rho_p$                         | $\text{kg m}^{-3}$         |
| Plume density contrast                 | $\Delta\rho_p = \rho_a - \rho_p$ | $\text{kg m}^{-3}$         |
| Plume viscosity                        | $\mu_p$                          | $\text{Pa s}$              |
| Plume volume flux                      | $Q$                              | $\text{m}^3 \text{s}^{-1}$ |
| Plume buoyancy flux                    | $B_p/g = \Delta\rho_p Q$         | $\text{kg s}^{-1}$         |
| <b><u>Initial Variables</u></b>        |                                  |                            |
| Slab initial bending lengths           | $l(0), l_b(0)$                   | $\text{cm}$                |
| Initial dip angle of the slab          | $\theta_0$                       | degrees                    |
| Time of plume initiation               | $t_p^i$                          | $\text{s}$                 |
| Plume source position relative to slab | F, R, S                          |                            |

Table S1.1: Experimental variables. F, R, and S refer to Front, Rear and Side initial plume position relative to the slab, respectively.

677 *S1.2. Dimensional analysis*

678 Discarding the initial variables, the system depends on the 11 following  
 679 primary variables:  $g, \mu_a, H, \Delta\rho_s, \mu_s, U, W, d, l, \mu_p$ , and  $B_p/g = \Delta\rho_p Q$ , and  
 680 has three fundamental dimensions (mass, length and time). We note that  
 681 the dynamics of subduction has been shown not to depend on the length of  
 682 the plate  $L$  (Li and Ribe, 2012). Consequently, according to the Buckingham  
 683  $\Pi$  theorem, the system depends on 8 dimensionless numbers. Dimensional  
 684 analysis then yields

$$\mathcal{F}\left(\frac{gd}{U^2}, \frac{\mu_a}{\Delta\rho_s U d}, \frac{H}{d}, \frac{\mu_s}{\Delta\rho_s U d}, \frac{W}{d}, \frac{l}{d}, \frac{\mu_p}{\Delta\rho_s U d}, \frac{B_p/g}{\Delta\rho_s U d^2}\right) = 0, \quad (1)$$

685 which we can rewrite

$$\mathcal{G}\left(\frac{U^2}{gd}, \frac{\Delta\rho_s U d}{\mu_a}, \frac{H}{d}, \frac{\mu_s}{\mu_a}, \frac{W}{d}, \frac{l}{d}, \frac{\mu_p}{\mu_a}, \frac{\Delta\rho_s U d W}{B_p/g}\right) = 0, \quad (2)$$

686 OR

$$\mathcal{G}\left(Fr, Re, \frac{\mu_s}{\mu_a}, \frac{\mu_p}{\mu_a}, \frac{H}{d}, \frac{W}{d}, \frac{l}{d}, \frac{B_s}{B_p}\right) = 0, \quad (3)$$

687 using the definition of the slab buoyancy flux  $B_s/g = \Delta\rho_s U W d$ , and iden-  
 688 tifying that the two first dimensionless groups in equation 2 are the Froude  
 689 number and Reynolds number, respectively. Equation 3 points out that one  
 690 important dimensionless number of the problem is the slab/plume buoyancy  
 691 flux ratio. Now, physical considerations point out that the system could also  
 692 depend on the initial position tip of the slab, and hence the stiffness of the  
 693 plate  $S$  (see Suppl. Inf. S2 for further details), the time of plume initiation,  
 694 and the plume relative to the slab, for which a formal variable cannot simply  
 695 be defined. We will show that the subduction dynamics ultimately does not  
 696 depend on the tip initial conditions whereas the plume initial conditions will  
 697 impact on the nature of the interaction.

698 **S2. Appendix. Supplementary Material: Experimental Analyses**

699 *S2.1. Extent of the slab-induced poloidal and toroidal cell at the surface*

| Experiment    | $\gamma$ | $l$             | $r_F$           | $r_R$             |
|---------------|----------|-----------------|-----------------|-------------------|
| 3 (Slab-only) | 836      | 8 cm (40 km)    | 33 cm (1650 km) | 2 cm (100 km)     |
|               |          | 16 cm (800 km)  | 48 cm (2400 km) | 10 cm (500 km)    |
|               |          | 32 cm (1600 km) | 62 cm (3100 km) | 19 cm (950 km)    |
| 4             | 610      | 8 cm (40 km)    | 43 cm (2150 km) | <2.5 cm (<125 km) |
|               |          | 16 cm (800 km)  | 52 cm (2600 km) | 10 cm (500 km)    |
|               |          | 32 cm (1600 km) | 68 cm (3400 km) | 16 cm (800 km)    |
| 12            | 538      | 8 cm (40 km)    | 34 cm (1700 km) | <2 cm (<100 km)   |
|               |          | 16 cm (800 km)  | 40 cm (2000 km) | 12 cm (600 km)    |
|               |          | 32 cm (1600 km) | 61 cm (3050 km) | 19 cm (950 km)    |

Table S2.1: Extent of the slab-induced poloidal and toroidal flow seen at the surface as a function of slab length for three experiments. The distances  $r_F$  &  $r_R$  are estimated at the surface as the distances from the trench in the front and rear regions of the slab, where the slab-induced poloidal inflow (front region) and toroidal outflow (rear region) respectively vanishes.

700 Those distances  $r_F$  &  $r_R$  are estimates only as they are inferred from the  
701 displacement of the neutrally buoyant tracers that had been seeded at the  
702 surface, but they give a good indication of where plumes can be influenced  
703 by the slab once arrived at the surface. Regardless of the slab length, front  
704 plumes will likely be caught in the poloidal flow from thousands of kilometres  
705 away from the trench, whereas rear plumes will not be affected by the toroidal  
706 flow unless they are close to the trench or the slab is long.



707 *S2.2. Initial tip length  $l$ , Bending length  $l_b$ , Stiffness  $S_0$  and sinking regimes*

708 As the plate was systematically bent initially from a length  $l_{top} = 3$  cm  
 709 measured from above as shown in Figure S2.1a, the initial tip length  $l(0)$  was  
 710 calculated as

$$l(0) = \frac{l_{top}}{\cos(\theta_0)}, \quad (1)$$

711 where  $\theta_0$  was the initial angle the slab made with the surface as shown in  
 712 Figure S2.1b. As  $l_{top}$  and  $\theta_0$  were measured within a maximum error of 0.2  
 713 cm and 3 degrees, respectively,  $l(0)$  was estimated within a typical error of  
 714 7%.

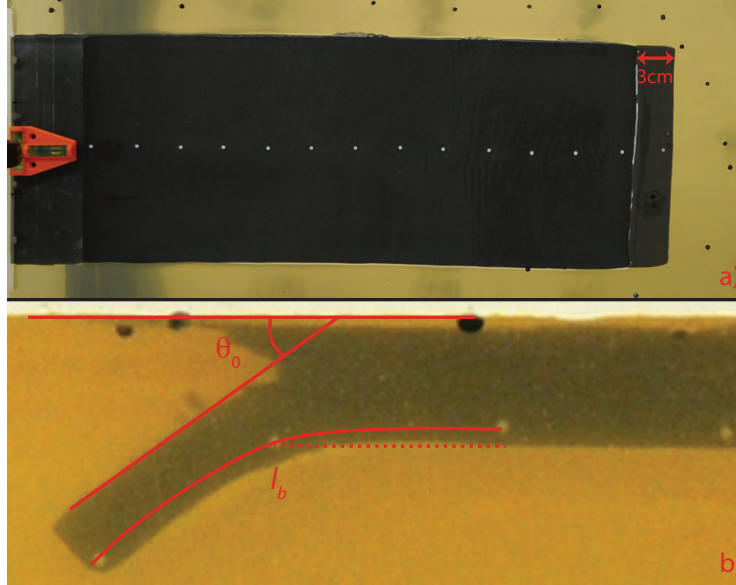


Figure S2.1: a) Initial slab tip seen from above. b) Close-up of Initial slab tip seen from the side showing the initial dip angle of the slab  $\theta_0$ , and the length of curvature  $l_b(0)$ . Note that the distance between the white markers was 4 cm.

715 The initial bending length  $l_b(0)$  was measured to within 5% from the  
 716 photos of the side-view as shown in Figure S2.1b. For experiments 3 & 13-18,

717 however, the initial plate curvature could not be seen. We attribute this to  
718 an initial smaller curvature, equivalently larger radius of curvature and hence  
719 larger initial bending length  $l_b(0)$  of these latter experiments compared to the  
720 other experiments, which can be explained by their larger  $\gamma$  ratio (up to a  
721 factor 1.6) (Schellart, 2010; Capitanio and Morra, 2012).

722 The initial plate stiffness  $S_0$ , defined by

$$S_0 = \gamma \left( \frac{d}{l_b(0)} \right)^3 \quad (2)$$

723 was then estimated for experiments 1-2, 4-12 & 19-21, for which  $l_b(0)$  could  
724 be estimated. Values of  $S_0$  are greater than 3, which suggests that the ob-  
725 served sinking regime would initially not be in a Stokes dominated regime  
726 but rather in the transition between a Stokes dominated regime and a stiff-  
727 ness dominated regime (Ribe, 2010; Li and Ribe, 2012). Consequently, for  
728 experiments 3 & 13-18, it cannot be excluded that the larger values of  $l_b(0)$   
729 resulted in a smaller value of  $S_0 \lesssim 3$ , and hence, compared with experiments  
730 1-2, 4-12 & 19-21, may have not initially been as dependent on the bending.  
731 Yet as sinking proceeds, the slab length  $l$  and the slab bending length  
732  $l_b$  increase with time. The plate stiffness defined by  $S = \gamma(d/l)^3$  is thus to  
733 decrease with time and the steady sinking rate is consequently expected to  
734 settle in the Stokes regime, in which  $U$  varies as  $\mu_a^{-1}$  (Li and Ribe, 2012).

735 *S2.3. Profiles of the tip vertical position as a function of time for experiments*  
736 *at buoyancy ratio  $\approx 15$*

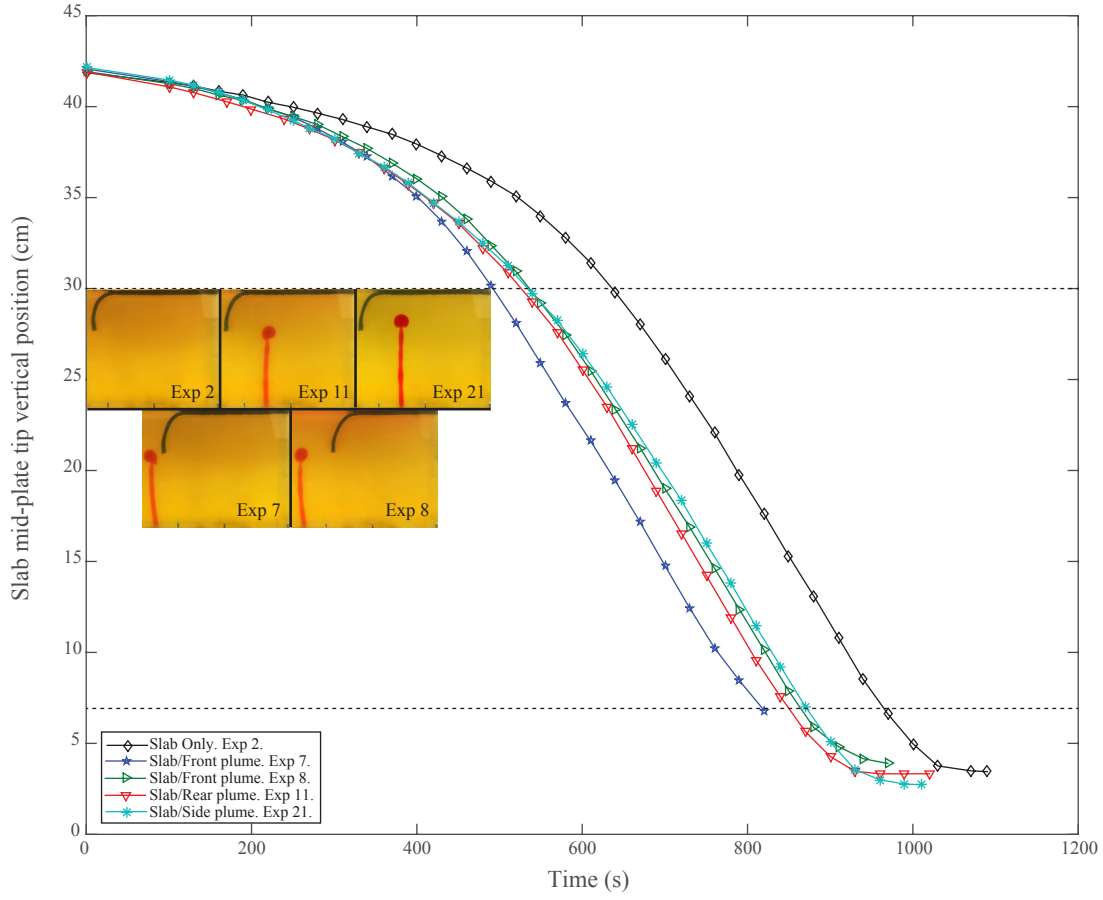


Figure S2.2: Slab tip vertical positions as a function of time for the slab only experiment 2 and, slab and Front, Rear and Side plume experiments 7, 8, 11 & 21, respectively. The two dashed lines indicate the two vertical positions between which linear regressions on the slab tip positions were made to determine the slab steady sinking rates  $U$  given in Table 1. The five inserts show the slab and plume positions when the slab tip is at the vertical position of 30 cm from where the linear regressions start.

737 *S2.4. Estimates of  $F_b$  and  $F_p$ .*

| Experiment | $l(t_p^s)$ | $A(t_p^s)$        | $F_p$                   | $F_b$                   | $F_p/F_b$ |
|------------|------------|-------------------|-------------------------|-------------------------|-----------|
|            | (m)        | (m <sup>2</sup> ) | (kg m s <sup>-2</sup> ) | (kg m s <sup>-2</sup> ) | %         |
| 14         | 0.04       | 0.0408            | 0.0135                  | 0.0471                  | 29        |
| 15         | 0.12       | 0.0276            | 0.0311                  | 0.1413                  | 22        |
| 18         | 0.08       | 0.0554            | 0.0200                  | 0.0942                  | 21        |

Table S2.2: Vertical forces  $F_b$  and  $F_p$  at the time  $t_p^s$  of plume spreading initiation underneath the plate.

738 *S2.5. Plume tilts*

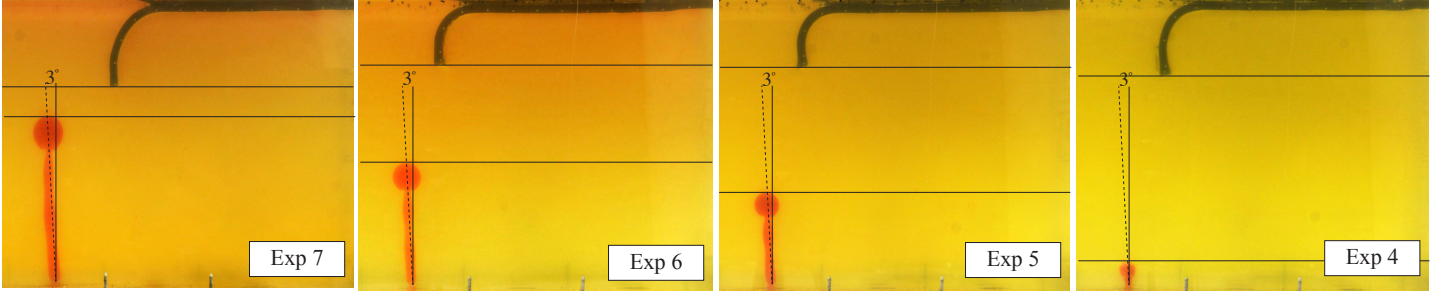


Figure S2.3: Snapshots of slab/plume positioning for experiments 4, 5, 6 & 7, from bottom to top, at the time the plume is tilted by three degrees to the vertical.

739 During its ascent, a plume responds to the ambient shear, and assuming  
 740 horizontal shear, the angle  $\alpha$  of tilt in the direction of shear from the vertical  
 741 at some depths follows a simple relationship between the shear velocity  $U_s$  at  
 742 that depth, and the plume Stokes velocity  $U_p$  (Richards and Griffiths, 1988)

$$\tan \alpha \approx \frac{U_s}{2U_p}, \quad (3)$$

743 which can be related to the plume buoyancy  $B_p$  (Kerr & Mériaux, 2004)  
 744 leading to

$$\tan \alpha \approx \frac{U_s}{2} \frac{\sqrt{\mu_a/\mu_p}}{k\sqrt{8B_p/\pi\mu_a}}, \quad (4)$$

745 where  $k$  for compositional plumes has a value of 0.54 (Richards and Grif-  
 746 fiths, 1988). According to equation 4, a shear 2-3 times larger was necessary  
 747 to achieve the same tilt on the plume between experiments 4 and 7, or equiv-  
 748 alently the ambient slab-induced shear velocity  $U_s$  increases with height by  
 749 at least a factor 2-3. The shear rate estimates represented 1.4 to 3% of the  
 750 sinking rates between experiments 4 and 7.

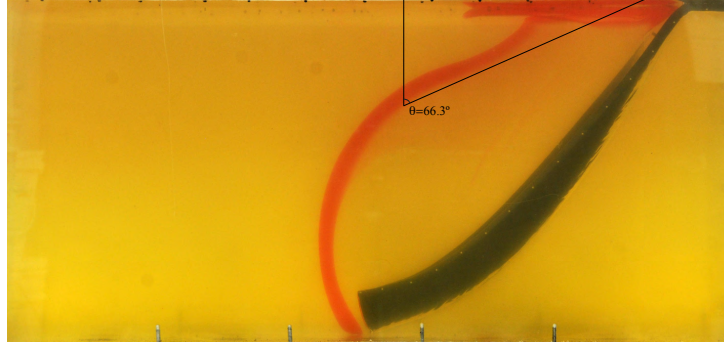


Figure S2.4: Maximum tilt of  $66.3^\circ$  encountered in the first 14 cm (700 km) from the surface in experiment 8.

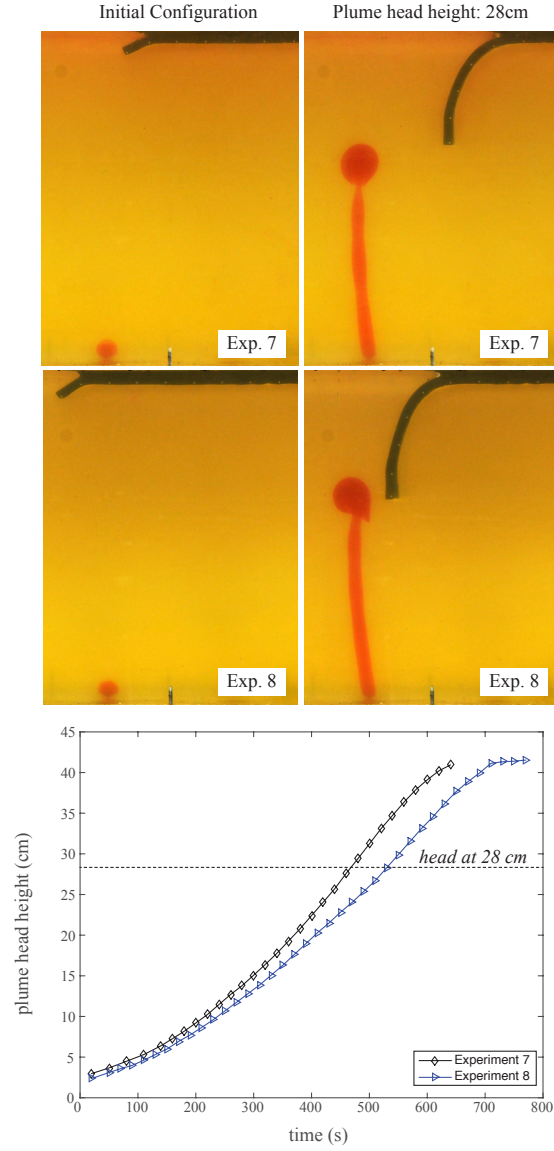


Figure S2.5: Experiments 7 & 8 of similar  $B_s/B_p$ : 1) Plume and slab initial configuration (top left photos), 2) Plume and slab configuration shown when the plume head is at 28 cm (top right photos), and 3) Plume head vertical height as a function of time.

752 **S3. Appendix. Supplementary Material: Application to Nature.**

753 *S3.1. Range of slab/plume buoyancy flux ratios  $B_s/B_p$  in nature.*

| <i>Nature</i>  | $W$  | $d$  | $\Delta\rho_s$       | $U$     | $B_s/g$                    | $B_p/g$ | $B_s/B_p$ |
|--|------|------|----------------------|---------|----------------------------|---------|-----------|
|  | (km) | (km) | (kg/m <sup>3</sup> ) | (cm/yr) | $\times 10^5(\text{kg/s})$ | (kg/s)  |           |
| Fast & Very wide subduction zone/Weakest plume           | 7000 | 75   | 80                   | 10      | 1.42                       | 200     | 710       |
| Fast & Very wide subduction zone/Medium plume            | 7000 | 75   | 80                   | 10      | 1.42                       | 1000    | 355       |
| Fast & Very wide subduction zone/Strongest plume         | 7000 | 75   | 80                   | 10      | 1.42                       | 6400    | 142       |
| Fast & Wide subduction zone/Weakest plume                | 1000 | 75   | 80                   | 10      | 0.71                       | 200     | 101       |
| Fast & Wide subduction zone/Medium plume                 | 1000 | 75   | 80                   | 10      | 0.71                       | 1000    | 51        |
| Fast & Wide subduction zone/Strongest plume              | 1000 | 75   | 80                   | 10      | 0.71                       | 6400    | 20        |
| Fast & Narrow subduction zone/Weakest plume              | 400  | 75   | 80                   | 10      | 0.28                       | 200     | 40        |
| Fast & Narrow subduction zone/Medium plume               | 400  | 75   | 80                   | 10      | 0.28                       | 1000    | 20        |
| Fast & Narrow subduction zone/Strongest plume            | 400  | 75   | 80                   | 10      | 0.28                       | 6400    | 8         |
| Medium speed & Very wide subduction zone/Weakest plume   | 7000 | 75   | 80                   | 5       | 0.20                       | 200     | 142       |
| Medium speed & Very wide subduction zone/Medium plume    | 7000 | 75   | 80                   | 5       | 0.20                       | 1000    | 71        |
| Medium speed & Very wide subduction zone/Strongest plume | 7000 | 75   | 80                   | 5       | 0.20                       | 6400    | 28        |
| Medium speed & Wide subduction zone/Weakest plume        | 1000 | 75   | 80                   | 5       | 0.10                       | 200     | 20        |
| Medium speed & Wide subduction zone/Medium plume         | 1000 | 75   | 80                   | 5       | 0.20                       | 1000    | 10        |
| Medium speed & Wide subduction zone/Strongest plume      | 1000 | 75   | 80                   | 5       | 0.20                       | 6400    | 4         |
| Medium speed & Narrow subduction zone/Weakest plume      | 400  | 75   | 80                   | 5       | 0.04                       | 200     | 8         |
| Medium speed & Narrow subduction zone/Medium plume       | 400  | 75   | 80                   | 5       | 0.04                       | 1000    | 4         |
| Medium speed & Narrow subduction zone/Strongest plume    | 400  | 75   | 80                   | 5       | 0.04                       | 6400    | 1.6       |
| Slow & Very wide subduction zone/Weakest plume           | 7000 | 75   | 80                   | 2       | 0.08                       | 200     | 22        |
| Slow & Very wide subduction zone/Medium plume            | 7000 | 75   | 80                   | 2       | 0.08                       | 1000    | 11        |
| Slow & Very wide subduction zone/Strongest plume         | 7000 | 75   | 80                   | 2       | 0.08                       | 6400    | 4.4       |
| Slow & Wide subduction zone/Weakest plume                | 1000 | 75   | 80                   | 2       | 0.04                       | 200     | 3.2       |
| Slow & Wide subduction zone/Medium plume                 | 1000 | 75   | 80                   | 2       | 0.04                       | 1000    | 1.6       |
| Slow & Wide subduction zone/Strongest plume              | 1000 | 75   | 80                   | 2       | 0.04                       | 6400    | 0.6       |
| Slow & Narrow subduction zone/Weakest plume              | 400  | 75   | 80                   | 2       | 0.0162                     | 200     | 1.3       |
| Slow & Narrow subduction zone/Medium plume               | 400  | 75   | 80                   | 2       | 0.0162                     | 1000    | 0.6       |
| Slow & Narrow subduction zone/Strongest plume            | 400  | 75   | 80                   | 2       | 0.0162                     | 6400    | 0.2       |

Table S3.1: Natural range of slab/plume buoyancy flux ratios on the basis of modern range of slab width, slab velocity and plume buoyancy. We have assumed constant values of  $d$  and  $\Delta\rho_s$ , which can vary but to a lesser degree. The buoyancy flux  $B_p$  for a medium plume is based on a statistical analysis (Mériaux et al., 2015b; Supplementary Information). The range of possible buoyancy flux ratios is 0.2–710.

754 S3.2. Some modern plumes in the vicinity of a trench.

755 S3.2.1. The Cascadia/Bowie and Cobb systems

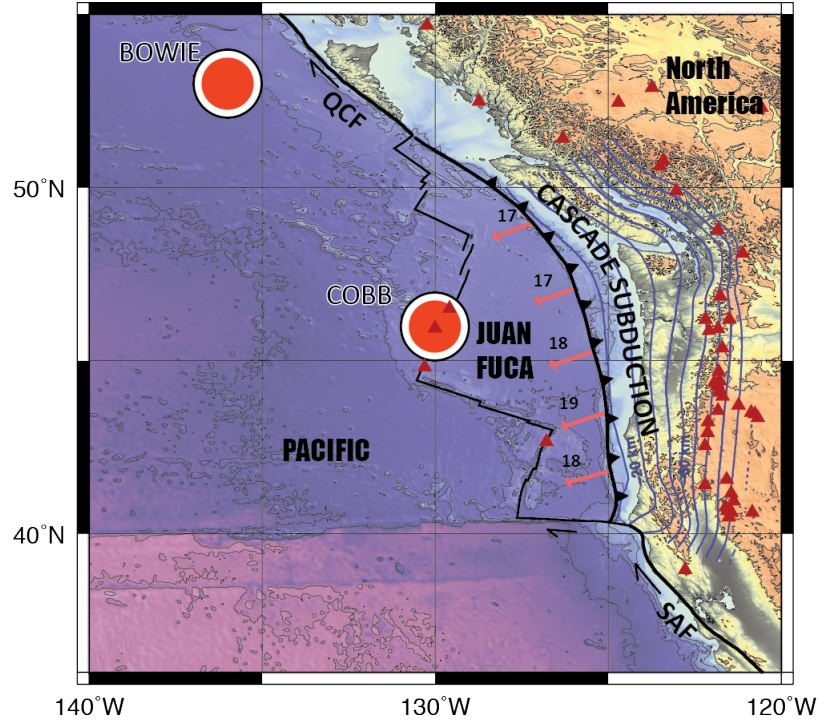


Figure S3.1: Bowie and Cobb hotspots in the vicinity of the Cascadia subduction zone. Topography and bathymetry with black contours every 1 km are from ETOPO1 [Amante and Eakins, 2009] . The red triangles are active volcanoes and the red arrows show the rollback of the cascade trench. Absolute velocities of the trench motions (in mm/yr) are calculated in the GSRM-APM-1 hotspot reference frame (Kreemer, 2009). Plate boundaries are modified from Bird (2003). SAF: San Andreas Fault, QCF: Queen Charlotte Fault. The slab surface is highlighted by blue contours at 10 km intervals (Hayes et al., 2012).



756 An additional movie named PlateKinematic-HS-since60Ma.m4v is pro-  
757 vided to show the plate reconstruction over the Bowie, Cobb and Yellow-  
758 stone plumes in the last 60 Ma, assuming that the three hotspots are as old.  
759 The conditions for slab/rear plume interactions might have only been met  
760 between 40-60 Ma for Bowie, and 45-60 Ma for Cobb, and involve the two  
761 subduction zones of Alaska and British Columbia where the Kula plate sub-  
762 ducted under North America (NA). Yet, at the time, plumes being located  
763 at least 900 km away from the nearest trench, only the slab-induced poloidal  
764 flow may have played a role in capturing the rear plume material towards  
765 the trench. Note the evolution of the Juan de Fuca subduction zone width  
766 over the last 30 Ma and the activation of the Queen Charlotte and San An-  
767 dreas strike-slip faults, north and south respectively of the Juan Fuca plate.  
768 The evolution of the Juan Fuca plate subduction also affected its interaction  
769 with the 16 Ma Yellowstone front plume. Overall, the complex geodynamic  
770 history of the region has likely resulted in some atypical spreading of plume  
771 material, which should encourage further geochemical/petrological and/or  
772 seismological investigations. All the plate reconstructions were made using  
773 GPlates 1.5 ([www.gplates.org](http://www.gplates.org)) using the plate boundaries and kinematics of  
774 Zahirovic et al. (2015).

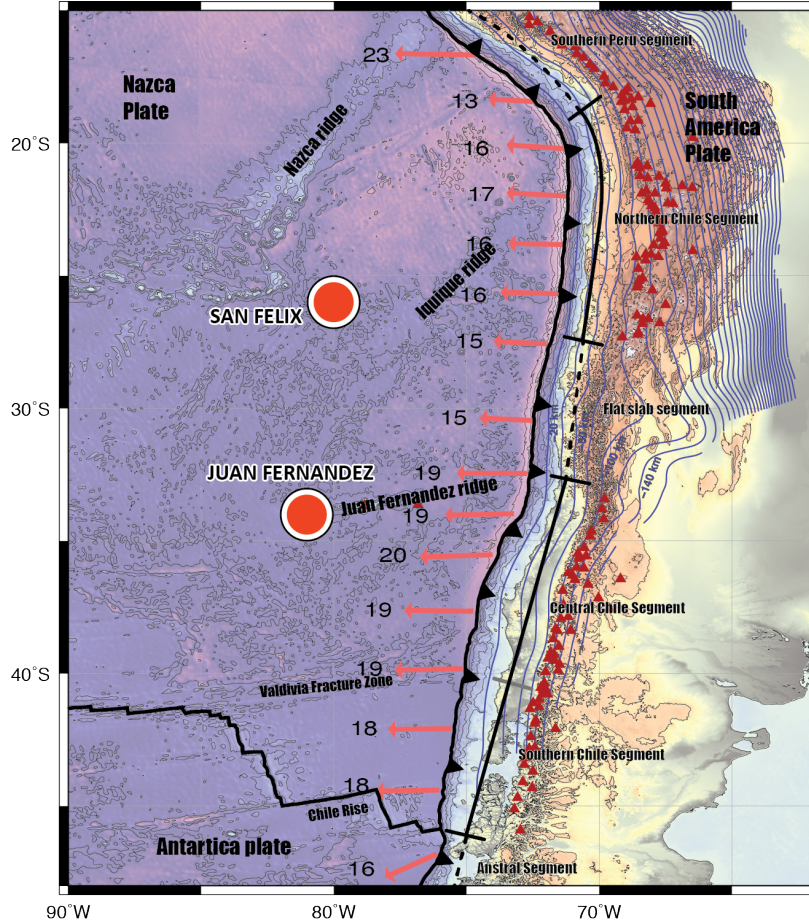


Figure S3.2: San Felix and Juan Fernández hotspots at the rear of two retreating segments of the South-American subduction zone. Topography and bathymetry with black contours every 1 km are from ETOPO1 [Amante and Eakins, 2009]. The red triangles are active volcanoes and the red arrows show the rollback of the Peru-Chile trench. Absolute velocities of the trench motions (in mm/yr) are calculated in the GSRM-APM-1 hotspot reference frame (Kreemer, 2009). Plate boundaries are from Bird (2003). The slab surface is highlighted by blue contours at 20 km intervals (Hayes et al., 2012). The two northern and southern shorter slab segments are indicated with the tick mark delimited black lines.

| <u>Slab/Plume systems</u>                    | Time | Mean Slab depth | Trench mode      | Plume/Trench Position | $R_{pt}$ | $B_p/g$   | $d$ | $U^{(a)}$ | $U_t^{(a)}$ | $W$   | $B_s/g$ | $B_s/B_p$ |
|--|------|-----------------|------------------|-----------------------|----------|-----------|-----|-----------|-------------|-------|---------|-----------|
|  | Ma.  | km              |                  |                       | km       | kg/s      | km  | cm/yr     | cm/yr       | km    | kg/s    |           |
| <u><b>This study</b></u>                     |      |                 |                  |                       |          |           |     |           |             |       |         |           |
| Cascadia/Bowie                               | 0    | 1200            | Retreating       | Rear/Side             | 320      | 600       | 35  | 2.2       | 1.8         | 1400  | 2,735   | 5         |
| Cascadia/Cobb                                | 0    | 1200            | Retreating       | Rear                  | 330      | 300       | 35  | 2.2       | 1.8         | 1400  | 2,735   | 9         |
| Nazca/San Felix                              | 0    | 600             | Quasi stationary | Rear                  | 820      | 1600-2300 | 80  | 2.7       | 0.7         | 6000  | 32,877  | 14-20     |
|  |      |                 |                  |                       |          |           |     | 3.5       | 0.5         | 910   | 6,464   | 3-4       |
| Nazca/Juan Fernández                         | 0    | 140             | Quasi stationary | Rear                  | 835      | 1600-1700 | 80  | 2.7       | 0.7         | 6000  | 73,059  | 14-20     |
|  |      |                 |                  |                       |          |           |     | 3.8       | 1.6         | 2940  | 22,673  | 10-14     |
| Java/South Java <sup>(b)</sup>               | 0    | 1000            | Retreating       | Rear                  | 150      | 1000      | 105 | 3.8       | 1.8         | 1700  | 17,207  | 17        |
| San Cristobal/East of Solomon <sup>(b)</sup> | 0    | 500             | Stationary       | Front                 | 700      | 1000      | 68  | 2.8       | 0.0         | 1450  | 7,000   | 7         |
| New Hebrides/Coral Sea <sup>(b)</sup>        | 0    | 400             | Retreating       | Rear                  | 1200     | 1000      | 85  | 5.2       | 6.6         | 1300  | 14,576  | 14        |
| <u><b>Previous studies</b></u>               |      |                 |                  |                       |          |           |     |           |             |       |         |           |
| Manila/Hainan                                | 0    | 670             | Retreating       | Rear                  | 1000     | 1000      | 65  | 3.1       | 2.3         | 5,112 | 10      | 5         |
| Gibraltar/Canary                             | -10  | 660             | Retreating       | Side                  | 150      | 290-570   | 75  | 2.5       | 2.0         | 400   | 1900    | 3-7       |
| Tonga/Samoa                                  | 0    | 1000            | Retreating       | Rear/Side             | 700      | 1600      | 120 | 6.8       | 6.8         | 3400  | 70,380  | 44        |
| Cascadia/Yellowstone                         | 0    | 1200            | Retreating       | Front                 | 1200     | 1500      | 35  | 2.2       | 1.8         | 1400  | 2735    | 2         |
|  | -15  | ?               | Retreating       | Front                 | 380      | 1500      | 44  | 2.6       | 2.3         | 2000  | 5,804   | 4         |

Table S3.2: Some plumes in the vicinity of a slab. <sup>(a)</sup> We note that modes and velocities may vary between the different absolute reference frames, (1) hotspot reference frame of Gripp and Gordon (2002), which analyses the Pacific hotspot track; (2) hotspot reference frame of Gordon and Jurdy (1986), which considers both the Indo-Atlantic and the Pacific hotspot tracks; (3) hotspot reference frame of Steinberger et al. (2004), which investigates only the Indo-Pacific hotspot tracks; (4) no-net-rotation reference frame (Gripp and Gordon, 2002), and (5) a subduction zone reference frame (Schellart, 2011). Here we have adopted subduction modes and subduction velocities of Schellart et al. (2011), and Schellart et al. (2010). <sup>(b)</sup> refers to lower mantle starting plumes. Today’s slab depths were taken from Hayes et al. (2012), Fukao and Obayashi (2013), and Gutscher et al. (2002).  $R_{pt}$  is an estimate of the distance between the trench and the plume. For  $B_p$ , we used values from Davies (1988), Sleep (1990), Steinberger (2000), and Courtillot et al. (2003). When not available, we used the buoyancy flux of 1000 kg/s for a medium plume based on a statistical analysis (Mériaux et al., 2015b; Supplementary Information).  $d$  was estimated from plate ages (Heuret and Lallemand, 2005) according to  $d$  (km)  $\sim 7 + 11 \times \sqrt{\text{age (Ma)}}$ . The sinking rate  $U$  was calculated from the along-trench averaged subduction rate assuming a slab dip angle of 45 degrees.  $U_t$  is the retreat rate. We have used the slab widths  $W$  of Schellart et al. (2007) given in the Supplementary Information and measured those which Schellart et al. (2007) did not provide. A value  $\Delta\rho_s$  of 80 kg/m<sup>3</sup> was used to calculate  $B_s/g$ .

776 *S3.3. Slab/plume systems from magmatism*

| Slab/Plume system                     | Age       | Volcanism   | Reference                      |
|---------------------------------------|-----------|---|--------------------------------|
| Abitibi- Wawa arc/plume               | ~ 2700 Ma | southern Superior Province                          | Wyman et al. (2002)            |
| Baltic arc/plume                      | ~ 2700 Ma | Sumozero-Kenozero greenstone belt                   | Puchtel et al. (1999)          |
| Paleo-Pacific arc/Karoo plume         | 270 Ma    | Patagonia calc-alkaline arc magmatism               | Rapela et al. (2005)           |
| East Asia Pacific arc/plume           | 140 Ma    | Adakitic arc  | Lee and Ryu (2015)             |
| Izu-Bonin-Mariana arc/Oki-Daito plume | 50 Ma     | Oceanic plateaus on the Philippine Sea plate        | Ishizuka et al. (2013)         |
|                                       |           | Benham Plateau                                      | Deschamps and Lallemand (2003) |
|                                       |           | Manus Basin   | Macpherson and Hall (2001)     |
| Cocos arc/Baja-Guadalupe plume (??)   | 10 Ma     | Mexican volcanic belt                               | Márquez et al. (1999)          |
| Ionian arc/Etna plume                 | 0 Ma      | Mount Etna  | Schiano et al. (2001)          |
| Tonga arc/Samoa plume                 | 14-0 Ma   | Volcanoes of Tafahi and Niuatoputapu, and Lau basin | Ewart et al. (1998)            |
| Cascadia arc/Yellowstone plume        | 17.5-0 Ma | Columbia plateau                                    | Geist and Richards (1993)      |

Table S3.3: Slab/plume systems where mixed plume and arc magmatism have been reported. This list is not exhaustive.

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